



# Supplement of

# Topographic metrics for unveiling fault segmentation and tectono-geomorphic evolution with insights into the impact of inherited topography, Ulsan Fault Zone, South Korea

Cho-Hee Lee et al.

Correspondence to: Yeong Bae Seong (ybseong@korea.ac.kr)

The copyright of individual parts of the supplement might differ from the article licence.

### Supplementary #1: Sensitivity analysis

We conducted sensitivity analysis to identify how the model input parameter affects the  $\chi$  and relief values and  $\chi$  anomaly and relief difference across the main drainage divide. We picked several values for the parameters that we want to test (i.e., *n*-channel slope exponent,  $\theta$ -channel concavity index, and *K*-erodibility coefficient). The values for each parameter that we tested are listed below (Table S1).

|               | Parameters |       |          |  |  |  |  |  |
|---------------|------------|-------|----------|--|--|--|--|--|
|               | n          | θ     | К        |  |  |  |  |  |
| Simulation 1  | 0.6494     | 0.36  | 1.00E-07 |  |  |  |  |  |
| Simulation 2  | 0.6494     | 0.65  | 1.00E-07 |  |  |  |  |  |
| Simulation 3  | 0.6494     | 0.505 | 1.00E-07 |  |  |  |  |  |
| Simulation 4  | 5.0419     | 0.36  | 1.00E-07 |  |  |  |  |  |
| Simulation 5  | 5.0419     | 0.65  | 1.00E-07 |  |  |  |  |  |
| Simulation 6  | 5.0419     | 0.505 | 1.00E-07 |  |  |  |  |  |
| Simulation 7  | 2.8457     | 0.36  | 1.00E-07 |  |  |  |  |  |
| Simulation 8  | 2.8457     | 0.65  | 1.00E-07 |  |  |  |  |  |
| Simulation 9  | 2.8457     | 0.505 | 1.00E-07 |  |  |  |  |  |
| Simulation 10 | 0.6494     | 0.36  | 1.00E-04 |  |  |  |  |  |
| Simulation 11 | 0.6494     | 0.65  | 1.00E-04 |  |  |  |  |  |
| Simulation 12 | 0.6494     | 0.505 | 1.00E-04 |  |  |  |  |  |
| Simulation 13 | 5.0419     | 0.36  | 1.00E-04 |  |  |  |  |  |
| Simulation 14 | 5.0419     | 0.65  | 1.00E-04 |  |  |  |  |  |
| Simulation 15 | 5.0419     | 0.505 | 1.00E-04 |  |  |  |  |  |
| Simulation 16 | 2.8457     | 0.36  | 1.00E-04 |  |  |  |  |  |
| Simulation 17 | 2.8457     | 0.65  | 1.00E-04 |  |  |  |  |  |
| Simulation 18 | 2.8457     | 0.505 | 1.00E-04 |  |  |  |  |  |

Table S1. The tested values for each parameter

About *n* (slope exponent), we selected its minimum value as 0.6494 and its maximum value as 5.0419 according to the previously calculated values for environments (e.g., rock type, climate, seismicity, tectonic activity, and the presence of glacier) similar to our study area (Harel et al., 2016). We also selected the median value (2.8457) between the minimum and maximum values. We selected the minimum value of  $\theta$  as 0.36 and maximum value as 0.65, following the previous research (Snyder et

al., 2000; Wobus et al., 2006; Cyr et al., 2010; Kirby and Whipple, 2012) and tested their median value (0.505) as well. Lastly, we selected the minimum value of *K* as 1.00E-07 because we used 5.56E-07 in this research, which is average value from the environments similar to this study area (Harel et al., 2016) so that we can find out whether we used quite uncertain value or not. The maximum value of *K* is selected as 1.00E-04, which is generally used in the reported cases (e.g., Stock and Montgomery, 1999; Kirby and Whipple, 2001; Zondervan et al., 2020).

We ran 72 landscape evolution models with the values in Table S1 for the configurations of all modelling cases (i.e., Cases A1, A2, B1, and B2). Then, we analysed topographic metrics ( $\chi$  index and relief) from the modelled topographies and calculated their anomalies. The metrics' values are documented in supplementary 2 (excel file), and we made some scatter plots to identify how those parameters affect the results.

#### 1. Influence of slope exponent (n)



Figure S1. Influence of slope exponent (*n*) on the  $\chi$  index,  $\chi$  anomaly, relief, and relief anomaly. The anomalies are the subtraction of the mean value of each metric on the eastern side from that on the western side. (a)  $\chi$  index, (b)  $\chi$  anomaly, (c) relief, and (d) relief anomaly variation on each tested *n* value.

It seems that the variation of *n* has very weak or no relationship with  $\chi$  index,  $\chi$  anomaly, and relief anomaly (Figs. S1a, S1b, and S1d). However, relief (Fig. S1c) generally increases as *n* increases.

### 2. Influence of channel concavity index $(\theta)$



Figure S2. Influence of channel concavity index ( $\theta$ ) on the  $\chi$  index,  $\chi$  anomaly, relief, and relief anomaly. The anomalies are the subtraction of the mean value of each metric on the eastern side from that on the western side. (a)  $\chi$  index, (b)  $\chi$  anomaly, (c) relief, and (d) relief anomaly variation on each tested  $\theta$  value.

As  $\theta$  increases, both  $\chi$  index and relief decrease (Figs. S2a and S2b), and the range (both in positive and negative direction) of the  $\chi$  anomaly and relief anomaly also decrease (Fig. S2b and S2d).

## 3. Influence of erodibility coefficient (K)



Figure S3. Influence of erodibility coefficient (*K*) on the  $\chi$  index,  $\chi$  anomaly, relief, and relief anomaly. The anomalies are the subtraction of the mean value of each metric on the eastern side from that on the western side. (a)  $\chi$  index, (b)  $\chi$  anomaly, (c) relief, and (d) relief anomaly variation on each tested *K* value.

As *K* increases, the range of  $\chi$  anomaly increases (Fig. S3b), and both relief and the range of relief decrease (Figs. S3c and S3d).

# Supplementary 2

|               |        |        |          |             |                              | R                                  | esuitvalues                  |                               |                               |                               |                              |                              |  |  |
|---------------|--------|--------|----------|-------------|------------------------------|------------------------------------|------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------------|------------------------------|--|--|
|               | F      | aramet | ers      |             |                              | Modelling cases                    |                              |                               |                               |                               |                              |                              |  |  |
|               |        |        |          |             | A1                           |                                    | A2                           |                               | B1                            |                               | B2                           |                              |  |  |
| n             |        | tneta  | ĸ        |             | West                         | East                               | West                         | East                          | West                          | East                          | West                         | East                         |  |  |
| Simulation 1  | 0.6494 | 0.36   | 1.00E-07 | X<br>Relief |                              |                                    |                              |                               |                               |                               |                              |                              |  |  |
| Simulation 2  | 0.6494 | 0.65   | 1.00E-07 | X<br>Relief |                              |                                    |                              |                               |                               |                               |                              |                              |  |  |
| Simulation 3  | 0.6494 | 0.505  | 1.00E-07 | X<br>Relief |                              |                                    |                              |                               |                               |                               |                              |                              |  |  |
| Simulation 4  | 5.0419 | 0.36   | 1.00E-07 | X<br>Relief | 37.42 ± 2.14<br>33.25 ± 9.94 | 37.74 ± 2.56<br>32.08 ± 4.53       | 21.28 ± 1.53<br>25.95 ± 4.20 | 21.69 ± 1.54<br>27.11 ± 4.35  | 39.32 ± 1.91<br>34.36 ± 15.10 | 34.20 ± 2.31<br>35.45 ± 12.09 | 21.67 ± 1.81<br>26.02 ± 5.09 | 20.44 ± 1.54<br>27.04 ± 3.26 |  |  |
| Simulation 5  | 5.0419 | 0.65   | 1.00E-07 | X<br>Relief | 0.58 ± 0.06<br>1.48 ± 0.12   | 0.58 ± 0.05<br>1.48 ± 0.08         | 0.42 ± 0.05<br>1.48 ± 0.14   | 0.42 ± 0.05<br>1.43 ± 0.12    | 0.61 ± 0.07<br>1.45 ± 0.18    | 0.46 ± 0.06<br>1.50 ± 0.08    | 0.45 ± 0.06<br>1.44 ± 0.14   | 0.34 ± 0.06<br>1.49 ± 0.10   |  |  |
| Simulation 6  | 5.0419 | 0.505  | 1.00E-07 | X<br>Relief | 4.43 ± 0.40<br>7.65 ± 0.95   | 4.40 ± 0.34<br>7.39 ± 0.80         | 2.87 ± 0.27<br>6.23 ± 0.90   | 2.94 ± 0.34<br>6.27 ± 0.65    | 4.49 ± 0.36<br>7.70 ± 1.33    | 3.77 ± 0.31<br>7.67 ± 0.83    | 3.12 ± 0.28<br>6.42 ± 1.03   | 2.61 ± 0.27<br>6.45 ± 0.59   |  |  |
| Simulation 7  | 2.8457 | 0.36   | 1.00E-07 | X<br>Relief |                              |                                    | 19.21 ± 1.61<br>86.67 ± 7.98 | 24.52 ± 2.09<br>74.46 ± 17.15 |                               |                               |                              |                              |  |  |
| Simulation 8  | 2.8457 | 0.65   | 1.00E-07 | X<br>Relief | 0.59 ± 0.06<br>5.41 ± 0.39   | 0.56 ± 0.07<br>5.19 ± 0.35         | 0.44 ± 0.07<br>3.67 ± 0.34   | 0.42 ± 0.06<br>3.65 ± 0.34    | 0.60 ± 0.06<br>5.42 ± 0.52    | 0.47 ± 0.06<br>5.35 ± 0.33    | 0.48 ± 0.05<br>3.80 ± 0.35   | 0.34 ± 0.06<br>3.82 ± 0.30   |  |  |
| Simulation 9  | 2.8457 | 0.505  | 1.00E-07 | X<br>Relief | 4.46 ± 0.42<br>21.87 ± 2.95  | 4.45 ± 0.47<br>21.89 ± 2.92        | 2.89 ± 0.35<br>15.12 ± 1.99  | 3.02 ± 0.35<br>15.20 ± 0.83   | 4.49 ± 0.38<br>22.06 ± 4.31   | 3.61 ± 0.46<br>21.99 ± 1.61   | 3.14 ± 0.34<br>15.80 ± 2.47  | 2.63 ± 0.35<br>16.29 ± 2.10  |  |  |
| Simulation 10 | 0.6494 | 0.36   | 1.00E-04 | X<br>Relief | 38.92 ± 2.55<br>8.59 ± 1.24  | 44.82 ± 2.28<br>7.94 ± 0.44        | 17.17 ± 1.25<br>2.15 ± 0.26  | 27.21 ± 1.63<br>1.99 ± 0.21   | 41.58 ± 4.17<br>8.82 ± 1.07   | 34.25 ± 4.09<br>8.50 ± 0.98   |                              |                              |  |  |
| Simulation 11 | 0.6494 | 0.65   | 1.00E-04 | X<br>Relief | 0.51 ± 0.07<br>0.16 ± 0.06   | 0.89 ± 0.12<br>0.24 ± 0.03         | 0.32 ± 0.07<br>0.02 ± 0.004  | 0.73 ± 0.08<br>0.01 ± 0.002   |                               |                               |                              |                              |  |  |
| Simulation 12 | 0.6494 | 0.505  | 1.00E-04 | X<br>Relief | 4.66 ± 0.44<br>2.32 ± 0.27   | 5.28 ± 0.46<br>2.05 ± 0.13         | 2.54 ± 0.22<br>0.63 ± 0.04   | 3.95 ± 0.33<br>0.53 ± 0.03    | 5.05 ± 0.63<br>2.32 ± 0.28    | 3.79 ± 0.32<br>2.08 ± 0.16    | 3.29 ± 0.37<br>0.65 ± 0.04   | 3.26 ± 0.28<br>0.53 ± 0.02   |  |  |
| Simulation 13 | 5.0419 | 0.36   | 1.00E-04 | X<br>Relief | 36.46 ± 2.33<br>8.41 ± 2.89  | 36.71 ± 2.66<br>8.08 ± 1.80        | 20.55 ± 1.76<br>6.66 ± 1.07  | 21.51 ± 1.66<br>6.79 ± 0.91   | 37.69 ± 2.86<br>8.54 ± 2.88   | 35.33 ± 2.22<br>8.53 ± 2.43   | 21.62 ± 1.91<br>6.76 ± 1.61  | 20.90 ± 1.53<br>6.73 ± 0.56  |  |  |
| Simulation 14 | 5.0419 | 0.65   | 1.00E-04 | X<br>Relief | 0.55 ± 0.08<br>0.32 ± 0.04   | $0.60 \pm 0.06$<br>$0.30 \pm 0.03$ | 0.41 ± 0.06<br>0.32 ± 0.03   | 0.48 ± 0.05<br>0.30 ± 0.03    | 0.53 ± 0.08<br>0.30 ± 0.03    | 0.48 ± 0.06<br>0.31 ± 0.04    | 0.44 ± 0.06<br>0.31 ± 0.03   | 0.43 ± 0.06<br>0.31 ± 0.02   |  |  |
| Simulation 15 | 5.0419 | 0.505  | 1.00E-04 | X<br>Relief | 4.53 ± 0.32<br>1.66 ± 0.27   | 4.36 ± 0.41<br>1.67 ± 0.22         | 2.97 ± 0.18<br>1.56 ± 0.18   | 2.88 ± 0.28<br>1.53 ± 0.17    | 4.45 ± 0.30<br>1.65 ± 0.34    | 3.82 ± 0.40<br>1.70 ± 0.27    | 3.08 ± 0.23<br>1.55 ± 0.22   | 2.47 ± 0.29<br>1.61 ± 0.15   |  |  |
| Simulation 16 | 2.8457 | 0.36   | 1.00E-04 | X<br>Relief | 36.98 ± 1.88<br>7.99 ± 1.95  | 37.55 ± 2.29<br>7.93 ± 1.23        | 20.64 ± 1.54<br>5.70 ± 1.38  | 22.55 ± 1.52<br>5.69 ± 0.73   |                               |                               |                              |                              |  |  |
| Simulation 17 | 2.8457 | 0.65   | 1.00E-04 | X<br>Relief | 0.54 ± 0.07<br>0.23 ± 0.03   | 0.60 ± 0.06<br>0.22 ± 0.02         | 0.41 ± 0.04<br>0.23 ± 0.01   | 0.49 ± 0.05<br>0.22 ± 0.02    | 0.55 ± 0.10<br>0.21 ± 0.03    | 0.46 ± 0.05<br>0.23 ± 0.03    | 0.45 ± 0.05<br>0.22 ± 0.02   | 0.43 ± 0.05<br>0.22 ± 0.02   |  |  |
|               |        |        |          | X           | 4.60 ± 0.37                  | 4.50 ± 0.35                        | 2.91 ± 0.25                  | 2.91 ± 0.29                   | 4.56 ± 0.34                   | 4.05 ± 0.37                   | 3.05 ± 0.30                  | 2.64 ± 0.29                  |  |  |

|                    |                      |             |                | A           | nomalies |          |          |         |         |         |        |        |  |  |  |  |
|--------------------|----------------------|-------------|----------------|-------------|----------|----------|----------|---------|---------|---------|--------|--------|--|--|--|--|
| Descentary Occ     |                      |             |                |             |          |          |          |         |         |         |        |        |  |  |  |  |
|                    | 1                    | aramet      | ers            |             |          | La       | ases     |         |         |         |        |        |  |  |  |  |
|                    | n                    | theta       | к              |             | A1       | A2       | B1       | B2      |         |         |        |        |  |  |  |  |
| Simulation 1       | 0.6494               | 0.36        | 1.00E-07       | X           |          |          |          |         |         |         |        |        |  |  |  |  |
|                    |                      |             |                | Relief      |          |          |          |         |         |         | <br>   |        |  |  |  |  |
| Simulation 2       | 0.6494               | 0.65        | 1.00E-07       | X<br>Relief |          |          |          |         |         |         |        |        |  |  |  |  |
| Simulation 3       | 0.6494               | 0.505       | 1.00E-07       | X<br>Relief |          |          |          |         |         |         |        |        |  |  |  |  |
|                    |                      |             |                | v           | -0 3237  | -0.4072  | 5 1247   | 1 2324  | _       |         |        |        |  |  |  |  |
| Simulation 4       | 5.0419               | 0.36        | 1.00E-07       | Relief      | 1 1756   | -1 1637  | -1.0888  | -1 0255 |         |         |        |        |  |  |  |  |
|                    | in 5 5.0419 0.65     |             |                | v           | 0.0012   | 0.0013   | 0 1436   | 0 1100  |         |         |        |        |  |  |  |  |
| Simulation 5       |                      | 0.65        | 1.00E-07       | Relief      | 0.0003   | 0.0433   | -0.0533  | -0.0523 |         |         |        |        |  |  |  |  |
|                    |                      |             |                | v           | 0.0267   | -0.0680  | 0.7202   | 0.5057  |         |         |        |        |  |  |  |  |
| Simulation 6       | 5.0419               | 9 0.505     | 1.00E-07       | Relief      | 0.2585   | -0.0435  | 0.0248   | -0.0314 |         |         |        |        |  |  |  |  |
|                    |                      |             |                | v           | 0.2000   | -5 3102  | 0.0210   | 0.0011  |         |         |        |        |  |  |  |  |
| Simulation 7       | 2.8457               | 0.36        | 1.00E-07       | Relief      |          | 12 2103  |          |         |         |         |        |        |  |  |  |  |
|                    |                      | 457 0.65    |                | v           | 0.0261   | 0.0185   | 0 1389   | 0 1343  |         |         |        |        |  |  |  |  |
| Simulation 8       | mulation 8 2.8457    |             | 1.00E-07       | Relief      | 0.2254   | 0.0180   | 0.0717   | -0.0197 |         |         |        |        |  |  |  |  |
|                    | ation 9 2.8457 0     | 0.505       | 505 1.00E-07   | v           | 0.0083   | -0 1277  | 0.8811   | 0.5142  |         |         |        |        |  |  |  |  |
| Simulation 9       |                      |             |                | Relief      | -0.0101  | -0.0824  | 0.0689   | -0.4879 |         |         |        |        |  |  |  |  |
|                    |                      |             | 0.36 1.00E-04  | v           | -5 8943  | -10.0377 | 7 3338   | 0.1010  |         |         |        |        |  |  |  |  |
| Simulation 10      | 0.6494               | 0.36        |                | Relief      | 0.6549   | 0.1530   | 0.3200   |         |         |         |        |        |  |  |  |  |
|                    |                      |             |                | Y           | -0.3814  | -0.4118  |          |         |         |         |        |        |  |  |  |  |
| Simulation 11      | 0.6494               | 494 0.65    | 0.65 1.00E-04  | Relief      | -0.0783  | 0.0043   |          |         |         |         |        |        |  |  |  |  |
|                    |                      |             |                | Y           | -0.6229  | -1.4050  | 1.2657   | 0.0297  |         |         |        |        |  |  |  |  |
| Simulation 12      | 0.6494               | 0.505       | 1.00E-04       | Relief      | 0.2740   | 0.1059   | 0.2406   | 0.1168  |         |         |        |        |  |  |  |  |
| 0. 1               | mulation 13 5.0419 0 | .0419 0.36  |                | X           | -0.2514  | -0.9675  | 2.3603   | 0.7154  |         |         |        |        |  |  |  |  |
| Simulation 13      |                      |             | 1.00E-04       | Relief      | 0.3321   | -0.1287  | 0.0047   | 0.0251  |         |         |        |        |  |  |  |  |
| 0. 1               | 5 0 1 40             | .0419 0.65  | 4.005.04       | X           | -0.0512  | -0.0735  | 0.0464   | 0.0144  |         |         |        |        |  |  |  |  |
| Simulation 14 5.04 | 5.0419               |             | 1.00E-04       | Relief      | 0.0145   | 0.0171   | -0.0034  | 0.0065  |         |         |        |        |  |  |  |  |
| 0. 1               | 5 0 4 4 0            | 0.505       | .505 1.00E-04  | X           | 0.1660   | 0.0960   | 0.6294   | 0.6092  |         |         |        |        |  |  |  |  |
| Simulation 15      | 5.0419               |             |                | Relief      | -0.0117  | 0.0243   | -0.0585  | -0.0534 |         |         |        |        |  |  |  |  |
| Simulation 16 2.   | 0.0457               | 7 0.36      | .36 1.00E-04 F | X           | -0.5659  | -1.9062  |          |         |         |         |        |        |  |  |  |  |
|                    | 2.8457               |             |                | Relief      | 0.0557   | 0.0088   |          |         |         |         |        |        |  |  |  |  |
| Cinculation 47     | 0.0457               | C7 0.00     | 0.05           | 0.05        | 0.05     | 0.05     | 1 005 04 | Х       | -0.0594 | -0.0797 | 0.0962 | 0.0222 |  |  |  |  |
| Simulation 1/      | 2.0457               | 0.65        | 1.000-04       | Relief      | 0.0167   | 0.0092   | -0.0188  | 0.0003  |         |         |        |        |  |  |  |  |
| Cimulation 40      | 2 9457               | 0.677 0.695 | 0.505 4.0      | 1 005 04    | Х        | 0.0990   | 0.0073   | 0.5042  | 0.4096  |         |        |        |  |  |  |  |
| Simulation 18      | 2.0457               | 0.505       | 1.00E-04       | Relief      | 0.0775   | 0.0726   | 0.0140   | 0.0255  |         |         |        |        |  |  |  |  |
|                    |                      |             |                |             |          |          |          |         |         |         |        |        |  |  |  |  |

\* About the shaded simulation cases, distance between the channel heads on the one side and another side are so far that they are not recognized as a paired basins. \* The anomaly is the difference between the mean of each metric on the western and eastern flank (mean value on the western flank minus mean value on the eastern flank).