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Quantifying the controls on potential soil production rates: a case study of the San Gabriel Mountains, California

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Table S1. Data used in the paper. Sample ID, location, elevation (z), mean slope (S_{av}), P values, and soil thickness (h) are from Heimsath et al. (2012).

Sample ID	Latitude (°)	Longitude (°)	z (m)	S_{av} (°)	P (m/Myr)	P error (m/Myr)	h (cm)	P_r (m/Myr)	P_r error	D (m/m)	$P_{r,pred}$ (m/Myr)
SG-1	34.2090	-117.7714	1072	30	300	38	0	300	38	24.8	174
SG-2	34.2118	-117.7685	1072	30	240	19	0	240	19	25.6	174
SG-6	34.1868	-117.7632	947	35	460	148	0	818	263	24.5	522
SG-7	34.1856	-117.7662	950	35	373	34	5	427	39	23.1	522
SG-10	34.207	-117.7621	855	18	68	5	38	221	16	26.4	154
SG-101	34.2852	-118.1519	1673	35	156	32	0	278	57	19.0	522
SG-102	34.2852	-118.1519	1673	35	251	51	30	564	115	19.0	522
SG-103	34.3717	-118.0710	2015	26	78	17	23	159	35	8.3	169
SG-104	34.3717	-118.0710	2015	26	21	9	30	53	23	8.3	169
SG-105	34.3707	-118.0701	2005	26	48	12	43	182	46	8.0	169
SG-106	34.3706	-118.0692	1990	26	51	13	36	156	40	9.2	169
SG-107	34.3569	-118.0631	1804	26	164	29	15	261	46	9.2	169
SG-108	34.3543	-118.0580	1625	26	113	23	15	180	37	9.1	169
SG-110	34.2931	-118.0199	1725	26	106	20	10	145	27	18.9	169
SG-111	34.2930	-118.0202	1721	26	63	15	44	246	59	19.1	169
SG-112	34.2932	-118.0211	1729	26	44	9	27	102	21	18.7	169
SG-113	34.2908	-118.0218	1650	26	44	10	34	126	29	19.6	169
SG-115	34.2832	-118.0263	1390	15	138	33	10	188	45	20.5	145
SG-153	34.3273	-117.7998	2194	29	90	18	20	167	33	24.7	173
SG-154	34.3460	-118.0060	1800	12	43	10	44	168	39	16.1	133
SG-155	34.3469	-118.0059	1790	12	50	13	54	267	69	16.1	133
SG-156	34.3476	-118.0061	1780	12	12	3	45	48	12	16.1	133
SG-200	34.3586	-117.9922	1710	13	68	13	16	112	21	15.8	137
SG-201	34.3589	-117.9920	1710	13	69	13	10	94	18	15.7	137
SG-202	34.3590	-117.9922	1706	13	72	13	15	115	21	15.7	137
SG-203	34.3592	-117.9923	1702	13	109	20	10	149	27	15.6	137
SG-07-009	34.3215	-118.0866	1132	15	69	12	28	164	29	8.6	145
SG-07-011	34.3320	-117.9483	2137	20	93	18	12	135	26	26.9	159
SG-07-012	34.3318	-117.9481	2128	20	84	17	20	156	32	27.1	159
SG-07-013	34.3318	-117.9481	2120	24	121	24	20	225	45	27.1	166
SG-07-014	34.3318	-117.9481	2115	24	156	32	24	328	67	27.1	166
SG-07-015	34.3259	-117.9517	1897	24	139	26	0	139	26	26.5	166
SG-07-016	34.3276	-117.9507	1965	24	130	25	0	130	25	29.6	166
SG-07-017	34.3304	-117.9498	2068	24	147	28	0	147	28	27.8	166
SG-07-019	34.3484	-118.0045	1773	12	10	2	49	46	9	18.2	133
SG-07-020	34.3482	-118.0035	1785	12	46	12	50	217	57	19.6	133
SG-07-021	34.3471	-118.0030	1802	12	71	16	35	210	47	18.3	133
SG-07-023	34.3627	-117.9108	1958	31	427	145	25	839	285	27.5	308
SG-07-024	34.3615	-117.9107	1912	31	315	61	5	360	70	27.2	308
SG-07-025	34.3614	-117.9110	1889	31	266	54	7	321	65	27.1	308
SG-07-031	34.3348	-117.9695	1973	21	210	41	13	314	61	23.6	161
SG-07-032	34.3348	-117.9695	1973	21	210	38	3	230	42	23.6	161
SG-07-033	34.3348	-117.9695	1973	21	92	18	20	171	33	23.6	161
SG-07-034	34.3348	-117.9695	1973	21	132	25	5	154	29	23.6	161
SG-07-035	34.3264	-117.9690	1703	21	146	28	3	160	31	29.5	161
SG-07-038	34.3307	-117.9700	1847	21	178	33	3	195	36	28.4	161
SG-07-041	34.3307	-117.9700	1847	21	83	15	12	120	22	28.4	161
SG-07-042	34.3307	-117.9700	1847	21	98	18	12	142	26	28.4	161
SG-07-044	34.3524	-117.8792	2077	23	143	26	0	143	26	27.4	165
SG-07-045	34.3521	-117.8791	2058	38	594	125	8	737	155	27.5	527
SG-08-100	34.3639	-117.8379	1934	31	79	16	25	155	31	33.3	308
SG-08-101	34.3648	-117.8383	1880	31	338	90	8	419	112	33.6	308
SG-08-102	34.3648	-117.8383	1880	31	329	69	10	430	90	33.6	308
SG-08-105	34.3712	-117.8581	2494	35	96	23	0	170	41	33.4	209
SG-08-106	34.3714	-117.8578	2491	35	118	25	0	210	45	33.4	209
SG-08-108	34.3720	-117.8571	2442	35	166	34	20	285	58	33.2	209
SG-08-110	34.3723	-117.8631	2398	32	163	31	5	187	35	32.6	206