

**Morphodynamic
modelling of a
mixed-energy tidal
inlet**

G. Herrling and C. Winter

Morphological and sedimentological response of a mixed-energy barrier island tidal inlet to storm and fair-weather conditions

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Abstract

The environment of ebb-tidal deltas between barrier island systems is characterized by a complex morphology with ebb- and flood-dominated channels, shoals and swash bars connecting the ebb-tidal delta platform to the adjacent island. These morphological features reveal characteristic surface sediment grain-size distributions and are subject to a continuous adaptation to the prevailing hydrodynamic forces. The mixed-energy tidal inlet Otzumer Balje between the East Frisian barrier islands Langeoog and Spiekeroog in the southern North Sea has been chosen here as an exemplary study area for the identification of relevant hydrodynamic drivers of morphology and sedimentology. We compare the effect of high-energy wave-dominated storm conditions to mid-term tide-dominated fair-weather conditions on tidal inlet morphology and sedimentology with a process-based numerical model. A multi-fractional approach with five graduated grain-size fractions between 150 and 450 microns allows the simulation of corresponding surface sediment grain-size distributions. Net sediment fluxes for distinct conditions are identified: during storm conditions, bed load sediment transport is generally onshore directed on the shallower ebb-tidal delta shoals whereas fine-grained suspended sediment bypasses the tidal inlet by wave-driven currents. During fair-weather the sediment transport mainly focuses on the inlet throat and the marginal flood channels. We show how the observed sediment grain-size distribution and the morphological response at mixed-energy tidal inlets are the result of both, wave-dominant less frequent storm conditions and mid-term tide-dominant fair-weather conditions.

1 Introduction

Tidal inlets at barrier island systems connect the open sea with the back-barrier tidal basin. Typically, they feature an ebb-tidal delta seawards and a flood-tidal delta landwards of a deep inlet throat that is bordered by shallow sandy shoals and marginal flood channels (Hayes, 1979). Both, tidal flow constriction through the narrow inlet and wave

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3.2 Model nesting and boundary conditions

A hierarchical cascade of five model grids from the Continental Shelf to the East Frisian Barrier Islands with decreasing spatial dimensions and increasing numerical resolutions has been set-up to derive water levels and wave climate at the study area. In particular storm surge simulations require large model domains as coastal surge is generated by wind drag effects and atmospheric pressure gradients acting over long distances at open sea. The largest model with grid cell resolutions of 8000 m covers the Continental Shelf in the North Atlantic Ocean to the North Sea. Eight harmonic tidal constituents are applied to generate the astronomic tide at the sea boundaries of the Continental-Shelf-Model (Verboom et al., 1992). It embeds the Wadden-Sea-Model with average grid sizes of 1200 m covering the entire North Sea from the Dutch coast in the South to Denmark in the North. The Wadden-Sea-Model, in turn, generates water level time series at the seaward boundary of the smaller Ems-Elbe-Model with grid resolutions of approx. 200 m. The latter is additionally forced at the seaward boundary by wave data observed at the research platform FINO1 located 45 km offshore in water depths of 30 m. The next smaller model covers the East Frisian Barrier Islands from Juist to Wangerooge with model grid resolutions of 60–120 m and supplies wave- and water level boundary conditions to the most detailed Tidal-Inlet-Model covering only Langeoog and Spiekeroog islands. At the end of the model cascade, this 3-dimensional model with 10 sigma-layers over the vertical is dedicated to simulate the sediment dynamics at the tidal inlet Otzumer Balje and adjacent beaches (Fig. 1). It consists of 140 000 active grid cells with average grid resolutions of 60 m and up to 20 m in the breaker-zones, assumed to be sufficiently resolved for proper generation of wave-induced longshore currents.

3.3 Model bathymetry

Model bathymetries, i.e. depth schematizations for each particular model (Sect. 3.2), have been assembled by interpolating measured data of sea bottom elevations onto

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curvilinear model grids. Near coastal sub- and intertidal areas are covered by data of the years 2006, 2005 and 2001 based on conventional sounding methods (Federal Maritime and Hydrographic Agency, BSH). Elevations of inter- and supratidal barrier island beaches are partly covered by beach profiles of the year 2007 or high-resolution airborne LIDAR scans that are spatially limited and available for the years 2008, 2007 and 2005 (Coastal Research Station belonging to Lower Saxony Water Management, Coastal Defense and Nature Conservation Agency, NLWKN).

3.4 Meteorological forcing

Storms in the central part of the North Sea are associated with low-pressure systems. During the here reproduced extreme storm event “Tilo” between 5 and 10 November 2007 with peak surge levels on 9 November 2007, maximal wind velocities of 33 ms^{-1} and mean wind directions of North-North-West were recorded offshore (Outzen et al., 2008). Surge inducing wind stress and horizontal atmospheric pressure gradients acted over a large fetch from the Arctic Sea across the entire North Sea superimposed by high astronomical tide. The storm surge simulations are forced by meteorological model data of the German Weather Service (DWD). Wind and atmospheric pressure fields are available at 1 h intervals and spatial resolutions of 7 km and 2.8 km as for the COSMO-EU and COSMO-DE models, respectively.

The simulation representing fair-weather hydrodynamic conditions is forced by time series of wind data measured at the research platform FINO1 (Federal Maritime and Hydrographic Agency, BSH). Real-time data between 7 and 15 June 2007 are imposed to the wave and hydrodynamic simulations to account for a meteorological forcing with non-stationary wind velocities and directions. The mentioned period was selected based on visual comparison of generated wind roses due to the selected and a 2 yr data-set. Thus the selected data does not fulfill long-time statistical correctness, but the overall distribution of wind directions and intensity are similar to the long-time trend. Wind directions of the selected data series are from the westerly sector with

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a short intermittent period of easterly winds. The selected data is suggested to be sufficiently representative to account for typical low-energy wind- and wave conditions.

3.5 Bed layer model for multiple sediment fractions

A dynamic bed layer model is applied permitting the re-distribution of multiple sand fractions in relation to imposed bed shear stresses. Thus it enables the computation of spatial distributions of surface sediment grain-size fractions and to evaluate arithmetic mean grain-sizes in response to different hydrodynamic conditions. Each sand fraction depletes or increases in the bed cell according to erosion or deposition processes in the sediment transport formulation. A coefficient according to each mass-percent is applied in the transport equation to account for the availability of the mobilized sand fraction at a given bed-cell. Thus, sediment transport occurs if the critical shear stress for a certain grain-size fraction exceeds while its load is additionally controlled by the relative availability of each fraction. For details on the set-up and functioning of the bed layer model it is referred to Van der Wegen et al. (2010).

Within this study, model simulations were restricted to a limited number of five non-cohesive sand fractions with grain-sizes of 150, 200, 250, 350 and 450 μm because of computational expenses.

At first, preliminary simulations with fair-weather and storm forcing conditions, respectively, were initiated with a spatially uniform distribution of 20 mass-percent each (Fig. 8). Thus, the initial arithmetic mean grain-size equals 280 μm throughout the model domain. As the focus is on the sediment dynamics at the tidal inlet, a characteristic gradation of rather coarse sediment fractions between 150 and 450 μm was selected. According to this grain-size configuration, areas exposed to a low-energy wave impact such as the back-barrier tidal flats or the lower shoreface are hence not subject to significant morphological changes and thus grain-size sorting processes. Here, the initial arithmetic mean surface sediment grain-size of 280 μm did not change significantly during the simulations, although significantly finer sediments may occur in nature. This circumstance is tolerated here because back-barrier sediment dynamics

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and exchange processes between the back-barrier basin and the foreshore are not in the focus of this study. Back-barrier tidal flats contain high amount of fine sand and cohesive sediments and would require a different model set-up and grain-size configuration.

In a second step, to allow for a more realistic schematization of the surface sediment grain-size distribution at the area of interest, three model simulations with alternating hydrodynamic forcing conditions have been carried out. A simulation of 5 months being forced by fair-weather boundary conditions is followed by a storm surge simulation and another period of 5 months of fair-weather conditions. Sediment mass-fractions at the end of each model run are turned over to the consecutive simulation. The ultimate distribution of grain-sizes at the end of this sequence of simulations has been used for model validation purposes (Sect. 4.3). In addition, it serves as the initial distribution of grain-size mass-fractions for all other scenario model simulations where morphological changes and sediment fluxes are in the focus of the study (Figs. 4–7).

3.6 Morphological acceleration factor

A morphological scale factor is applied to account for the acceleration of bed-level changes during updates at each hydrodynamic time step (Roelfink, 2006). By use of this method which aims to economize computational run time, hydrodynamic time scales are adapted to much longer time scales of morphological evolution. Within this study, a morphological acceleration factor (Morfac) of 20 is applied during a simulation of 17 tidal cycles between neap and spring tide (7 to 15 June 2007) in order to account for morphological changes that occur during approximately 5 months of fair-weather conditions. For the storm surge simulation no morphological acceleration has been applied (Morfac = 1).

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Helmholz Zentrum Geesthacht, HZG) that are overestimated by 17 % in the simulation. Significant wave heights of approximately 3.5 m that were measured in the surf-zone of Norderney at 9 November 2007 at 07:00 a.m. (Kaiser et al., 2008) are underestimated by 17 % in the simulation.

It shall be noted that no model calibration has been performed by bed roughness adaptation. The bed roughness has been set to a uniform, constant value over the model domain (Manning parameter 0.024); no locally adapted bottom roughness values have been set. In particular against this background, the hydrodynamic model results can thus be considered as sufficiently good.

4.2 Sediment dynamics and morphology

Time series measurements of suspended matter (SPM) concentrations observed at the tidal inlet Otzumer Balje during the storm surge peak on 9 November 2007 show hourly mean (maximal) values in the order of 35 (65) mg L^{-1} and 55 (95) mg L^{-1} for maximal flood- and ebb-tide currents, respectively, at 0.5 m below mean low water level (Badewien et al., 2009). The three finest sediment fractions incorporated in the model simulation (150, 200 and 250 μm) reveal hourly mean (maximal) SPM concentrations of 45 (70) mg L^{-1} during maximal flood-tide currents at 2 m below German datum at the location of the measuring pole. These SPM concentrations in the flood-directed inlet flow are due to nearshore wave-induced sand resuspensions and satisfactorily reproduced by the model. During ebb-tide, simulated maximal SPM concentrations of 2 mg L^{-1} are strongly underestimated with respect to measurements. This can be explained by the fact that fine sand (< 150 μm) and cohesive sediments that are typically flushed out of the backbarrier tidal flats during increased storm surge ebb-flows (Bartholomä et al., 2009; Cuneo and Flemming, 2000), are simply not incorporated in this model set-up. However, here, discrepancies are not relevant for this study, because the model is not applied to predict residual sediment rates between the foreshore and backbarrier basin.

Observations of morphological changes as a response to the storm surge event of 9 November 2007 are available for two cross-shore profiles at the foreshore of Langeoog

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three alternating model runs with hydrodynamic forcings due to fair-weather conditions, storm conditions and again fair-weather conditions (Sect. 3.5).

The initial bathymetry of the detailed tidal inlet model is based on bathymetrical data of the years 2006/2007 and thus different from the inlet morphology of the sediment sampling campaign of 2005, here indicated by isolines based on available bathymetrical data of the years 2004/2005 (Fig. 3). The different morphological background explains the westerly bend of the channel through the ebb-tidal delta for the sampling state compared to a more straightened orientation in the model bathymetry.

Modeled and measured arithmetic mean surface sediment grain-size distributions show distinct similarities (Fig. 3). Surface sediments are coarsest at the inlet channel, the ebb-tidal delta and the eastern ebb-tidal delta shoal where swash bars migrate onshore. The central part of the ebb-tidal delta with medium to coarse sands is divided by a characteristic South–North oriented pattern of finer mean grain-sizes shown by both modeled and measured distributions. At the foreshore, modeled mean grain-sizes are generally coarser with respect to measurements.

The performance of the model to predict surface sediment grain-sizes increases for areas where the morphological changes are significant and thus sorting of sand fractions can take place. This may explain the discrepancies with respect to measured data at the foreshore. At the western ebb-delta shoals, on the other hand, distinct grain-size patterns of medium sand being predicted by the model cannot be validated by field data as the distance between sample positions (approx. 280 m) is too large in order to properly resolve these spatial patterns in surface sediment grain-sizes.

5 Results

Two model simulations are shown to compare the effect of an extreme storm surge event in the North Sea to a medium-term period (circa 5 months) of representative fair-weather conditions on morphodynamics and sedimentology at the tidal inlet Otzumer Balje between the barrier islands Langeoog and Spiekeroog.

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parallel to the shore and thus deviate from shore-oblique sand bars (Fig. 7b). At the north-eastern edge of the ebb-tidal delta shoal, shore-oblique sand bars connecting the eastern ebb-tidal delta with the downdrift surf-zone migrate eastwards under storm conditions. A sediment distribution with coarser grain-sizes at the bedform crests with respect to the troughs is predicted for the swash-bars as well as for the shore-oblique sand bars (Fig. 8b).

At the shoreface, fine sand fractions are winnowed and eroded in the troughs between and at the landward slopes of shoreface-connected sand ridges being located in water depths of 15–20 m below German datum (Fig. 8b). Fine sand tends to accumulate on the crests and the seaward slopes of the shoreface-connected ridges. Thus the shoreface-connected ridges experience a positive morphological feedback and a downdrift migration (Fig. 7b).

6 Discussion

The main drivers determining the morphodynamic equilibrium of a mixed-energy tidal inlet system are commonly assumed to be waves which induce sediment stirring, transport and dispersal at the ebb-tidal delta and tidal-currents in the inlet (e.g.: De Swart and Zimmerman, 2009; FitzGerald et al., 2012). Mixed energy barrier island tidal inlets are morphologically highly dynamic environments where both drivers continuously interact. Numerical model scenario experiments allow the separation of processes and boundary conditions for in-depth system understanding. However, a potential model approach that either reduces the forcing to tides or waves alone would be misleading as the natural interaction at mixed-energy tidal inlets would be ignored. Instead, here, tide- and wave-dominated forcing conditions are represented by realistic fair-weather and storm scenarios, respectively, which allow the evaluation of the morphological and sedimentological responses to distinct hydrodynamic drivers by preserving the mixed-energy regime of the system at the same time.

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For typical mixed-energy tidal inlets, it is commonly assumed that ebb-tidal delta erosion during episodic storm events counteracts the continuous replenishment of the ebb-tidal delta lobe during tide-dominated fair-weather conditions (FitzGerald et al., 2012; Hayes, 1979). This study does reproduce and thus confirms this hypothesis: Model simulations of mid-term fair-weather conditions reveal that the morphological activity mainly focuses on the inlet throat. Eastward littoral drift along the foreshore beaches supplies fine sands into the inlet throat. In the deep inlet channel, bed shear stress due to tidal currents is strong enough to remove fine sands. As residual sediment fluxes in the seaward part of the inlet throat are ebb-directed the entrained fine sands mainly feed the ebb-tidal delta. During storm conditions, wave refraction and shoaling over steep bottom gradients focus wave energy towards the ebb-tidal delta lobe and its shallow shoals where energy dissipates due to wave breaking. Here, the fine sand deposited during fair weather periods is easily mobilised and transported eastwards by the ambient flow, dominated by alongshore velocity components induced by high-energy waves. These waves, approaching in an angle with respect to the shore, generate alongshore momentum flux that is greatest in the zone of breaking waves (Longuet-Higgins and Stewart, 1964).

Sediment grain-size sorting mechanisms and thus the spatial distribution of surface sediments are related to bed shear stress controlled by wave- and tide-induced flow: Residual distributions of surface sediment grain-sizes make clear that both, storm conditions with high-energy waves and fair-weather conditions where tidal currents dominate, contribute to the sedimentology of barrier island tidal inlets and foreshore. At the tidal inlet, for instance, we can generalize that winnowing of fine sand at the inlet throat and marginal channels is attributed to tidal forcing, whereas high-energy waves are the driver for sorting mechanisms at shallow shoals of the ebb-tidal delta (Fig. 8). Simulations have shown that only the combined scenario forcing, i.e. alternating fair-weather and storm simulations, result in a surface sediment grain-size distribution that is in fair agreement with sedimentological field observations at Otzumer Balje inlet (Fig. 3; Son et al., 2010). On its own, this gives evidence that the combination of both hydrodynamic

parent to a minor grade, however major transport is through the ebb-dominated inlet throat and the flood-dominated eastern marginal channel. Hence, we conclude that – at least for the here studied tidal inlet – a significant re-circulation of sand to the inlet is only possible as a combination of both fair-weather and storm conditions.

Another aspect addresses the mentioned sediment bypass at the Otzumer Balje inlet. Son et al. (2010) suggest that there is no evidence for fine sand bypassing the tidal inlet. If at all, bypassing would take place along the subtidal margin of the terminal lobe and be independent of processes acting on the ebb-tidal delta. However, no evidence was given to support this hypothesis, as no data was collected from regions seaward of the ebb-tidal delta. In disagreement to the hypothesis of Son et al. (2010), our simulations reveal sediment bypass to the downdrift beach and foreshore for both, moderate and extreme conditions. The magnitude of the bypass, seaward extent and the dominant grain-size are primarily controlled by wave-energy, i.e. wave-induced longshore currents, and consequently are increased for storm with respect to fair-weather conditions.

The question whether the net volume of sand that is re-circulated to the inlet throat is dominant over the bypassed quantity must be answered by future studies, as the simulated scenarios are either representative for tide- or wave-dominated conditions but non-representative for the long-term regime of this mixed-energy tidal inlet. Ongoing research aims to elucidate the sediment budget at the tidal inlet.

7 Conclusions

This study identifies residual sediment fluxes of particular grain-size fractions and related morphological and sedimentological responses of a mixed-energy tidal inlet system. We use a process-based numerical modeling system to differentiate the effects of either tide- or wave-dominant forcing. During storm conditions, the ebb-tidal delta loses sand through wave attack. For fair-weather conditions, the ebb tidal delta is replenished by ebb-directed residual sediment transports. The model simulations satisfactorily re-

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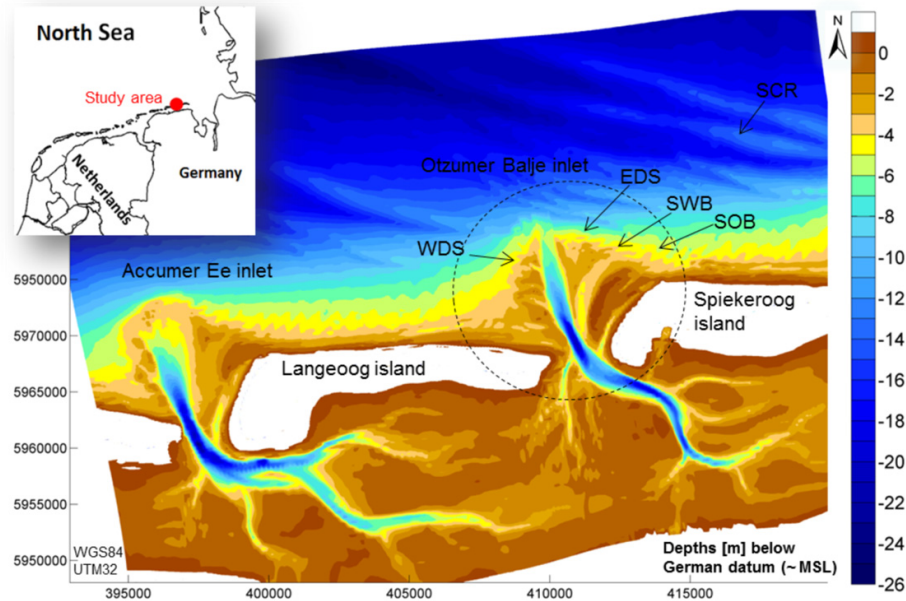


Fig. 1. East Frisian Barrier island system in the southern North Sea with the study area Otzumer Balje inlet between the islands Langeoog and Spiekeroog and nearshore morphological features such as the western/eastern ebb-tidal delta shoals (WDS/EDS), swash bars (SWB), shore-oblique sand bars (SOB) and shoreface-connected ridges (SCR).

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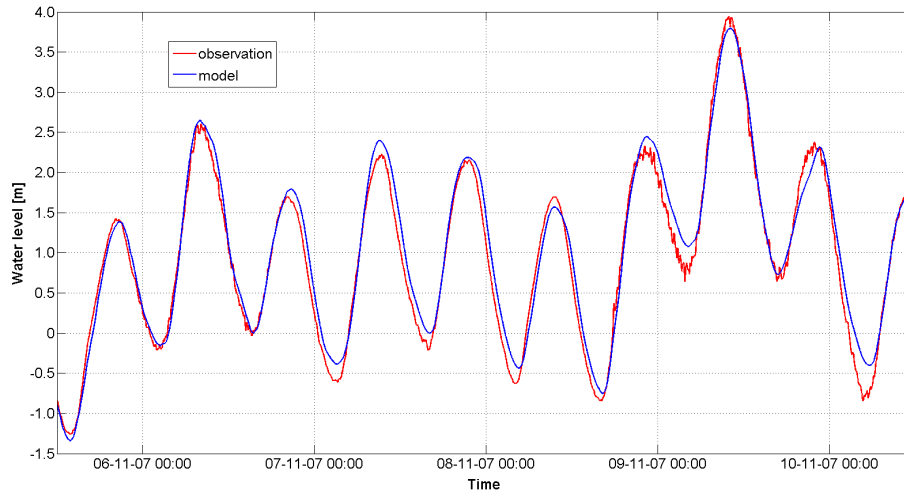


Fig. 2. Comparison of modeled (Delft3D-FLOW alone) and observed water level time series at water level gauge Spiekeroog for the storm event “Tilo” with peak surge levels on 9 November 2007.

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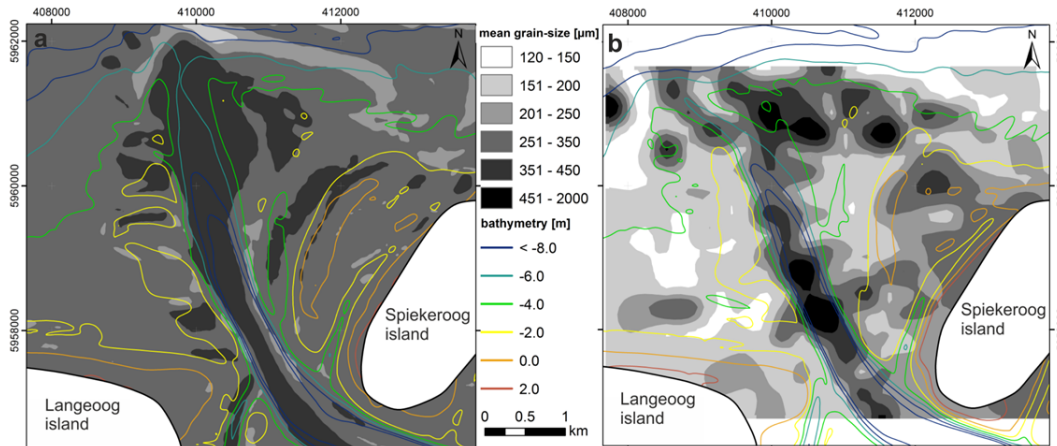


Fig. 3. Modeled (a) and measured (b) arithmetic mean surface sediment grain-size distributions at Otzumer Balje inlet between Langeoog and Spiekeroog islands; depths isolines based on bathymetrical data of 2006/2007 (a) and 2004/2005 (b).

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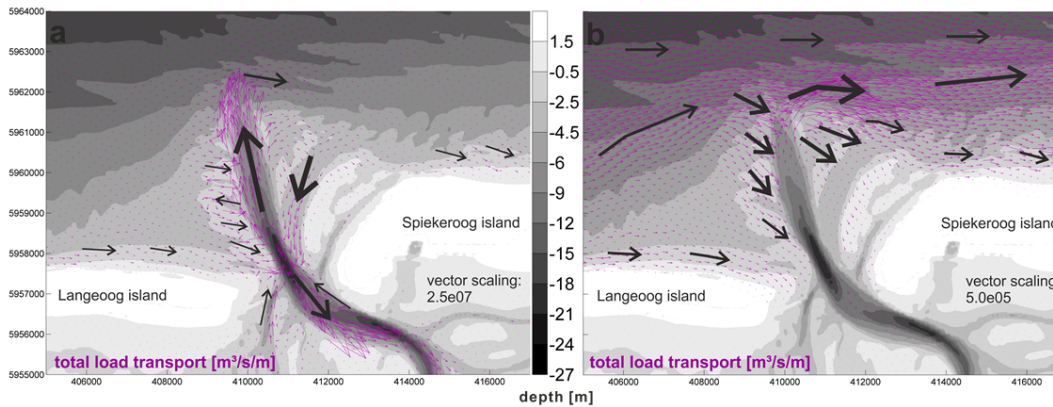


Fig. 4. Residual total load transport for fair-weather conditions **(a)** and storm conditions **(b)** and schematic main residual pathways indicated by black arrows.

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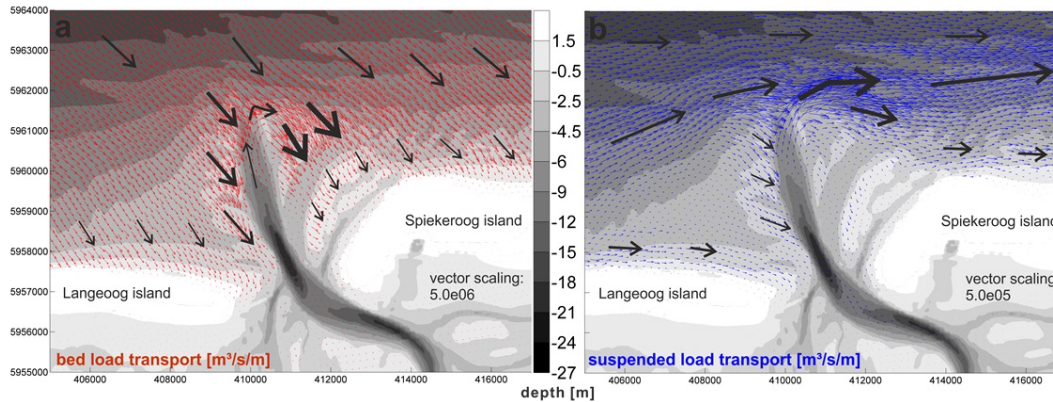


Fig. 6. Residual bed load **(a)** and residual suspended load **(b)** transport and schematic main residual pathways indicated by black arrows for high-energy storm conditions; relative vector scaling indicates suspended load to be about 10 times larger than bed load transport.

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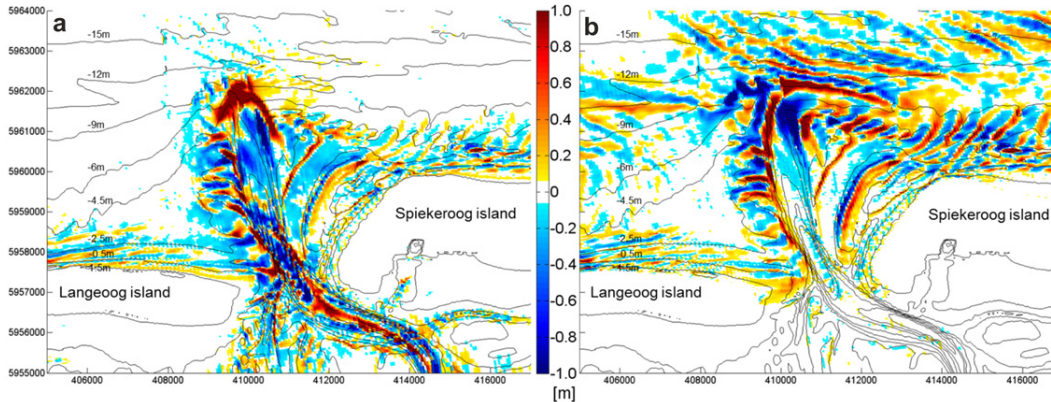


Fig. 7. Morphological changes, i.e. sedimentation (red) and erosion (blue) as a response to fair-weather (**a**) and storm (**b**) conditions; morphodynamic simulations have been initiated with already re-distributed surface sediment grain-size fractions (Fig. 3a).

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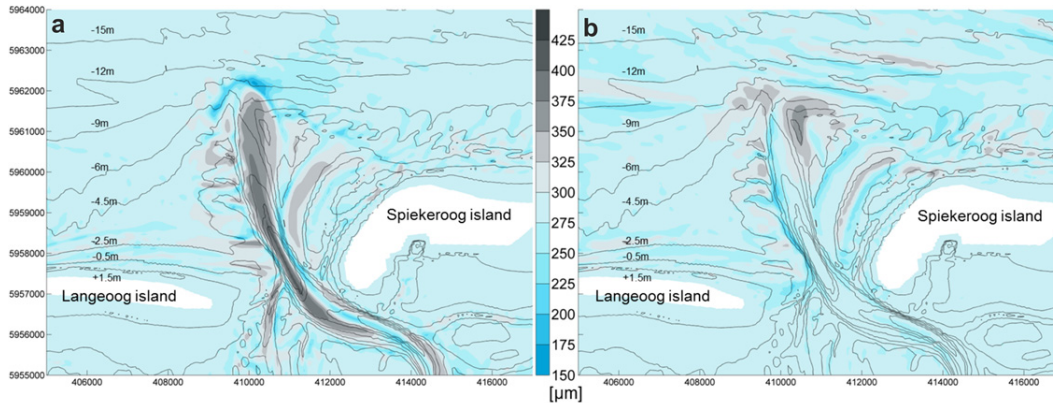


Fig. 8. Spatial distribution of arithmetic mean surface sediment grain-size as a response to fair-weather (**a**) and storm (**b**) conditions; simulations have been initiated with five equally distributed sand fractions of 150, 200, 250, 350 and 450 μm .

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