

Abstract

In the past few decades, many studies have been dedicated to our understanding of the interactions between tectonic and erosion and, in many instances, using numerical models of landscape evolution. Among the numerous parameterizations that have been developed to predict river channel evolution, the Stream Power Law, which links erosion rate to drainage area and slope, remains the most widely used. Despite its simple formulation, its power lies in its capacity to reproduce many of the characteristic features of natural systems (the concavity of river profile, the propagation of knickpoints, etc.). However, the three main coefficients that are needed to relate erosion rate to slope and drainage area in the Stream Power Law remain poorly constrained. In this study, we present a novel approach to constrain the Stream Power Law coefficients under the detachment limited mode by combining a highly efficient Landscape Evolution Model, FastScape, which solves the Stream Power Law under arbitrary geometries and boundary conditions and an inversion algorithm, the Neighborhood Algorithm. A misfit function is built by comparing topographic data of a reference landscape supposedly at steady state and the same landscape subject to both uplift and erosion over one time step. By applying the method to a synthetic landscape, we show that different landscape characteristics can be retrieved, such as the concavity of river profiles and the steepness index. When applied on a real catchment (in the Whataroa region of the South Island in New Zealand), this approach provide well resolved constraints on the concavity of river profiles and the distribution of uplift as a function of distance to the Alpine Fault, the main active structure in the area.

1 Introduction

Because their geometry is very sensitive to external forcing such as climate or tectonics, rivers are ideal natural laboratories to study the interactions of the various processes at play during orogenesis over geological time scales (Kirby and Whipple,

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2001, 2012; Montgomery and Brandon, 2002; Duvall et al., 2004; Whittaker et al., 2007). For this purpose many parameterizations of fluvial incision have been developed (Kooi and Beaumont, 1994; Sklar and Dietrich, 1998; Whipple and Tucker, 1999). The most widely used, the so-called Stream Power Law (SPL) (Howard, 1994; Whipple and Tucker, 1999), relates incision rate, \dot{e} to both drainage area A , a proxy for local discharge, and local slope S in the following manner:

$$\dot{e} = KA^m S^n \quad (1)$$

K is a proportionality coefficient called the “erosion efficiency” or “erodibility” that mostly depends on lithology and climate, while m and n are positive exponents that mostly depend on catchment hydrology.

Although the SPL is widely used in the community and has been implemented in various Landscape Evolution Models (LEMs) (Crave and Davy, 2001; Tucker et al., 2001; Braun and Willett, 2012), the values of K , m and n remain poorly constrained. These parameters, depend on numerous factors and cannot easily be measured from direct field observations. At best, one is commonly required to fix the value of one or two of them, to deduce the value of the other parameters from observational constraints (Stock and Montgomery, 1999; Kirby and Whipple, 2001). A more commonly approach is to compare the long-term predictions of a LEM with observational constraints on the rate of change of a given landform to infer the value of the SPL parameters (Van Der Beek and Bishop, 2003; Tomkin et al., 2003). However, most LEMs require a fine spatial and temporal discretization and are commonly limited by their computational cost (Tucker and Hancock, 2010). The use of inversion or optimization methods which require a thorough search through parameter space has been limited by these computational limitations. An alternative is to limit the computation and the comparison with observations to 1-D river profiles, as was done by Roberts and White (2010) in Africa and (Roberts et al., 2012) in the Colorado Plateau, to deduce information about the geometry and timing of uplift.

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In the past year, major advances have been made in improving the efficiency of the SPMs solving the SPL, and an algorithm has been developed (Braun and Willett, 2012) that is implicit in time and $O(n_p)$, i.e. computational time increase linearly with, n_p , the number of points used to discretize the landscape. This new algorithm, called

FastScape, is sufficiently efficient to be used inside an inversion procedure that requires tens of thousands of runs to search through parameter space, while still using a very high spatial discretization (10^8 nodes).

We present here a novel approach that we have developed to constrain the parameters of the Stream Power Law in environments that have reached geomorphic steady-state, i.e. a local equilibrium between uplift and erosion. The objective is to determine the best combination of the K , n and m parameters that will maintain a given landform in its starting geometry after applying a known or arbitrary uplift and eroding it according to the SPL. To achieve this we used the LEM FastScape combined with the Neighborhood Algorithm (NA) inversion method. We first applied our approach to a synthetic landscape for which the value of the SPL parameters are known to test its validity and usefulness. We then applied it to a Digital Elevation Model (DEM) from the Whataroa Valley in New Zealand, a region which has very likely reached geomorphic steady-state (Adams, 1980; Herman et al., 2010).

2 The erosion law

Using the SPL, we can predict river channel evolution in detachment-limited systems (bedrock rivers) undergoing constant and uniform uplift by using the following mass balance equation:

$$\frac{\partial h}{\partial t} = U - \dot{e} = U - KA^m S^n \quad (2)$$

where h is the elevation of the channel, t is time and U is rock uplift rate relative to a fixed or known base level (Whipple and Tucker, 1999). As explained above, to

constrain the exact value of K , m and n from natural landscapes is relatively complex. Their value is still debated and are likely to depend on the geomorphological, climatic and tectonic context but the following ranges are commonly admitted:

– $0 < m < 2$

– $0 < n < 4$

– K varies by several orders of magnitude as it depends on many factors such as lithology, climate, sedimentary flux or river channel width, but also on the value of the other two parameters m and n .

Assuming steady-state, an expression for equilibrium channel gradient or slope, S_e , can be easily obtained from Eq. (2):

$$S_e = \left(\frac{U}{K}\right)^{1/n} A^{-m/n} = k_s A^{-\theta} \quad (3)$$

which shows that, in situations where an equilibrium between uplift and incision has been reached, one can obtain information about the ratio $\theta = m/n$, by simply computing the relationship that must exist between drainage area and local slope. The results of such studies are numerous and yield values in the range $\theta = 0.35\text{--}0.6$ (Whipple and Tucker, 1999; Whipple, 2004; Kirby and Whipple, 2012). This ratio is called the concavity as its value is mostly constrained by the concavity of river profiles. The other parameter, k_s , relating equilibrium slope to drainage area is called the “steepness index”. Its use is a direct consequence of our realization that erodibility can only be constrained where uplift rate is known or, more exactly, that we should focus on constraining the relative response of a river to tectonic uplift, not its intrinsic erosional efficiency.

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3 Combining FastScape and NA

As stated earlier, we used the FastScape algorithm (Braun and Willett, 2012) to solve the SPL and predict landscape evolution in a given tectonic and geomorphic setting. The efficiency and stability of this algorithm make it well suited to be used inside an inversion scheme which requires a large number of model runs. As seen previously, the number of parameters used in the SPL (K , m and n) is relatively small but combined with the unknown uplift rate U and the fact that each parameter varies over a relatively wide range of values makes an exhaustive search through parameter space a rather tedious exercise that would require a large number of forward runs. Consequently we attempted to minimize the computational cost by using the *Neighborhood Algorithm* (NA) (Sambridge, 1999a, b), an inversion method that is well adapted to solve non-linear problems. This optimization method is based on 2 separate stages. The first one called the “sampling” stage consists in finding an ensemble of best fitting models (combinations between U , K , m and n) that reproduce well the observed data or, in our case, that maintain the landscape at steady-state. The second one called the “appraisal” stage consists in deriving quantitative and statistically meaningful estimates of each parameter from the ensemble of models generated in the first stage.

In order to compare the observed or reference landscape with the predicted one, one needs to construct a misfit function. In our case, we consider that both landscapes must have reached steady-state ($\partial h / \partial t = 0$). We use the observed or reference landscape as starting condition for the LEM to which we apply a uniform uplift increment; we then compute the resulting erosion over a time step of length Δt . We define the misfit, ϕ , as the square root of the $L2$ -norm of the change in height between observed h_{obs} and predicted h_{pred} topographies over the time step, Δt :

$$\phi = \sqrt{\sum_{i=1}^N \frac{(h_{i, \text{pred}} - h_{i, \text{obs}})^2}{\Delta t^2 \cdot U_{\text{obs}}^2}} \quad (4)$$

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be able to retrieve not only the value of the ratio $\theta = m/n$, which has already been demonstrated to be controlled by the concavity of river profiles, but the exact value of each of the two exponents, m and n too.

4.2 n , m and K are free

5 In this case we assume that the uplift rate, U , is known only and we fix it to the value used to construct the reference model by driving FastScape to steady-state. The results from the sampling stage show several important points (Fig. 3a). First, the reduction of the misfit function leads to a trade-off between the m and n . All models runs that have a common m/n ratio of 0.4 are characterized by the smallest misfit values; they appear
 10 in the first panel of Fig. 3a as a red line. Note that this ratio between m and n is the same as the one used to compute the reference landscape ($m/n = 0.4/1.0$). Second, the absolute minimum is not located at these values for m and n , as shown by the PDFs shown in Fig. 3b. Thus, if we do not know the erodibility, K , we cannot retrieve the values of the m and n exponents, only their ratios as demonstrated by previous
 15 slope-area studies by Lague et al. (2000) and Snyder et al. (2000). Third, the other two scatter plots of Fig. 3a show that there is also a trade-off between $m - n$ and K . The same low value of the misfit function can be achieved with high values for K and small values of both m and n , or, conversely, with small values of K and large values of m and n in their permissible ranges. Note that K varies logarithmically along the vertical
 20 axis. This is easily explained by the asymptotic behavior of the SPL in the vicinity of $m = n = 0$:

$$\frac{\partial h}{\partial t} = U - KA^0S^0 = U - K \quad (6)$$

which shows that steady-state can only be reached when $K = U$, where $U = 5 \times 10^{-4}$ is the uplift rate imposed to compute the steady-state reference landscape.

25 The abrupt termination of the alignment (or line) of red circles in Fig. 3a is an artifact of the range imposed on K . To produce small misfit landscapes for values of m and n

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larger than 0.6 and 1.5, respectively, would require values of K that are smaller than the smallest value permitted, i.e. 10^{-6} .

4.3 n , m , K and U are free

In this case, all parameters m , n , K and U are left free during the inversion. The scatter plots illustrating the behavior of the misfit function as a function of m , n and K are shown in Fig. 4 and are very similar to those of Fig. 3a. The ratio between m and n is properly retrieved and converges towards the imposed value of 0.4. The other scatter plots indicate that the uplift rate is poorly constrained and that no clear relationship can be evidenced between the parameter U and the other parameters. This result clearly demonstrates that the ratio $\theta = m/n$ can indeed be constrained from a steady-state landscape but that neither K nor U nor independent values for m and n can be constrained because of the presence of a spurious solution to the problem corresponding to $m = n = 0$ and $K = U$. Moreover, if neither U nor K is constrained, their ratio itself is unconstrained nor is the steepness index, $k_s = (U/K)^{1/n}$.

We realize, however, that this result may depend on the way we have constructed the misfit function to compare the reference and predicted landscape. Other definitions of the misfit function could prove to be more constraining, especially concerning the steepness index. However, if we assume that the shape of the reference or observed landform is the only information we possess, the definition of the misfit function we have used here makes full use of the information content of the observables and it is difficult to see how it could be improved.

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5 Application to the Whataroa catchment

5.1 Tectonic, climatic and geomorphic context

The Southern Alps, New Zealand are the surface expression of the on-going oblique collision between the Australian and Pacific plate (DeMets et al., 1990; Norris et al., 1990). This zone is characterized by very high uplift rates of up to 10 km yr^{-1} on the West side of the orogen (Wellman, 1979; Tippett and Kamp, 1993; Batt et al., 2000). This results in part from the high rate of convergence between the two plates ($8\text{--}12 \text{ mm yr}^{-1}$) and in part from the strong orographic control on precipitations that results in precipitation rate of the order of $10\text{--}13 \text{ myr}^{-1}$ on the west coast of the island, in comparison to the much dryer climate of the east coast (1 myr^{-1}) (Griffiths and McSaveney, 1983).

We focus our study on the Whataroa catchment (Fig. 5), which is located in the central Southern Alps along the West Coast and presents ones of the highest uplift rates in the region ($\approx 6\text{--}8 \text{ mm yr}^{-1}$) (Tippett and Kamp, 1993; Herman et al., 2010). The profile of the Whataroa River can be divided in 3 distinct zones which correspond to different erosional and depositional environments or mechanisms (Herman and Braun, 2006). At high elevations the dominant mechanism is glacial erosion. Between elevations of 200 and 1200 m, the valley cross-section is markedly V-shaped, which indicates that the river is incising or in a “detachment-limited” state. Below 200 m elevation, the river dynamics changes drastically with the formation of large meanders and an array of braided channels during low flow periods, indicating that the river is in a “transport-limited” state, i.e. transporting sediments eroded in the upstream part of its catchment towards base level.

We have used the present-day topography of the Whataroa catchment area as initial and reference landscapes in our inversion scheme. For that, we used a DEM obtained from the SRTM3 mission (resolution of 3 arcsec). We corrected it for the presence of iso-elevation areas by using the geometry of the current drainage system. Using ESRI ArcGIS9.3, we modified the value of each of the pixels of the DEM by an infinitesimal

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amount that is inversely proportional to the discharge computed by using the “real” and thus known drainage geometry. In doing so, we ensure that the discharge computed by FastScape is done in accordance with the real drainage network. We only applied the inversion procedure to the pixels that have a computed drainage area superior to a critical area of 10^6 m^2 . In doing so, we impose that the elevation within the main river trunk and its main tributaries only are used to compute the misfit function. This prevents the potential bias which might be introduced by the parts of the landscape that is still glaciated and/or controlled by hillslope processes only. For consistency, we did not include the parts of the landscape that are below 200 m in elevation where the evolution of the landscape is likely to be transport-limited and where the SPL is unlikely to apply.

5.2 Inversion results**5.2.1 Constraint of the SPL**

We applied the inversion scheme to the Whataroa catchment, by letting three parameters free: m , n and K and imposing, for each of them, a range of values that is commonly admitted in the literature (see Table 1). The Whataroa catchment is potentially ideally suited to this exercise, as the lithology is relatively spatially invariant with surface rocks consisting mostly of the mildly metamorphosed Otago schists. The catchment being relatively small (15 km in length), it is characterized by a relatively uniform and high precipitation rate. This implies that K should be spatially uniform ($\partial K / \partial x = 0$), if we neglect the effect of fracturation. Its value is however, poorly constrained and we will assume that it can potentially vary by up to 9 orders of magnitude. We will assume that the uplift rate is well constrained by a broad range of thermochronological data to a mean value of 6 km Myr^{-1} (Tippett and Kamp, 1993; Batt et al., 2000; Herman et al., 2010) and is spatially uniform. The misfit function is identical to what we used for the synthetic cases and given by Eq. (4). The values of the NA parameters N_{init} , N_{it} and N_{runs} are given in Table 1.

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The results of the inversion (Fig. 6) show that the misfit function display a minimum for a constant ratio between the parameters m and n , in a very similar way to the results of the synthetic runs shown previously. The relationship between m and n that minimizes the misfit function is not so well defined, however. Two peaks characterize the PDFs (Fig. 6b) for m and n but these values must be considered with great care as the inversion is similarly attracted by the spurious solution corresponding to $m = n = 0$ as shown in the two panels of Fig. 6a that illustrate the behavior of the misfit function with K . It is interesting to note, however, that the optimum values for m and n , 0.3 and 0.5 respectively, are somewhat different from the extremum values allowed by the imposed ranges ($0.2 < m < 1.5$ et $0.4 < n < 2.5$) which could suggest that these values are potentially meaningful. Regardless of these considerations, It is the ratio of the two exponents, i.e. the concavity, that is best constrained at a value of 0.6. Similarly to the synthetic cases, no constrained can be obtained for the value of K as illustrated by the PDF of this parameter in the last panel of Fig. 6b.

As in the synthetic cases, the optimization method proves to be efficient in constraining the ratio m/n . For the Whataroa catchment and under the assumption that it is in geomorphic steady-state, the optimum value is found to be 0.6, which sits within the range of acceptable values but towards their upper bound.

5.2.2 Constraint on the uplift geometry

The distribution of uplift (and thus exhumation, under the assumption of geomorphic steady-state) in the vicinity of the Alpine Fault is a matter of debate (Braun et al., 2010). Low temperature thermochronology data from rocks exposed along the western side of the Southern Alps are commonly interpreted as evidence for an increase in exhumation rate towards the Alpine Fault (Tippett and Kamp, 1993). Higher temperature thermochronological data as well as first-order structural evidence that all of the structures east of and including the Alpine Fault are east dipping reverse faults imply that the uplift and exhumation rates should be maximum near the present-day divide and thus decrease towards the Alpine Fault (Braun et al., 2010).

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In order to test these two hypotheses, we allowed the uplift rate to vary linearly between the base of the Whataroa catchment near the Alpine Fault and the position of the main divide at the top of the catchment in such a way that either of the two scenarios can be reproduced by varying a single coefficient, α , introduced in the definition of the uplift rate function, $U(x)$:

$$U = 2(1 - \alpha)U_0 \left(1 - \frac{x}{L}\right) + 2\alpha U_0 \frac{x}{L} \quad (7)$$

where U_0 the mean uplift rate in the Whataroa catchment (6 km Myr^{-1}), L the distance between the Alpine fault and the main divide and x the position varying between 0 and L . In this expression, α varies between 0 and 1 corresponding to a maximum uplift rate near the Alpine Fault or the divide, respectively (Fig. 7). $\alpha = 0.5$ corresponds to a spatially uniform uplift rate.

In the following inversion, four parameters were left free: α , K , m and n . The results show that the values of the parameter α that best minimizes the misfit function and thus constrains the landscape to remain at steady-state all lie above 0.5. The PDF of α (Fig. 8) demonstrates that the geometry of the river profile of the Whataroa is best explained with α values 0.59 ± 0.004 . This implies that the uplift rate should be increasing away from the Alpine Fault in accordance with the suggestion made by Braun et al. (2010). This result must, however, be considered with much caution as it relies on our assumption that spatial variations in K can be neglected. Although the rock type and rainfall distribution are relatively uniform within the Whataroa catchment, the level of fracturation is highly variable and strongly increases towards the Alpine Fault as a result of the very large strain that have been accumulated at depth in the ductile regime and near the surface in the brittle regime by the Alpine fault and the adjacent 1–5 km wide region. It is therefore not unlikely that the asymmetry in uplift rate we evidence through our inversion of the topographic data is not real but an artifact of our assumption that K is uniform. We do not feel confident, however, about applying a similar treatment to K than we did for U , i.e. allowing it to vary linearly as a function to the Alpine Fault, as we have no hard constrain on its mean value, nor on how it

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catchment geometry, which is difficult to justify over such long periods of time. Although Roberts and White (2010) and Roberts et al. (2012) do not explicitly aim at containing the SPL coefficients, their study demonstrate that present-day river profiles can be re-produced with great accuracy using arbitrarily defined model parameters and therefore do not contain all the information necessary to constrain the SPL parameterization.

The study we present here is the first which considers the problem in 2-D and lets the SPL coefficients to vary over broad ranges in order to determine their best values in a quantitative manner. We also show that the method is able to retrieve information about the distribution of present-day uplift, even under the assumption of geomorphic steady-state.

6.3 The Stream Power Law

Although the SPL used in this study is able to reproduce many observations and natural processes (i.e. the concavity of river profiles to the migration of knickpoints), it must be regarded as a first-order parameterization of the integrated effects of river incision and, as such, cannot be expected to adequately represent the many and varied physical processes at play. For example, the SPL cannot include the effect of sediment being delivered to the river channel by hill-slope processes. In most of the Whataroa catchment, which is subjected to rapid tectonic uplift, valley sides are at the critical angle of repose, as indicated by their steep, V-shaped morphology (Herman and Braun, 2006) and supply vast quantity of sediments to the streams. Several formulations have been proposed to include the effect of sediment (both bed load and suspended load) on the erosional power of a stream, its transport capacity and the way sediment protects the bed from erosion (Beaumont et al., 1992; Sklar and Dietrich, 2001). Furthermore, tectonic uplift is accompanied by deformation and fracturing that is clearly evidenced by the intense hydrothermal activity in the vicinity of the Alpine Fault (Allis and Shi, 1995). The resistance of rocks to erosion is very likely to be strongly influenced by fracturing (Molnar et al., 2007) but it cannot be included in the SPL in a physically meaningful

manner; at best the coefficient K can be arbitrarily adjusted to represent the zeroth-order effect of fracturing on erodibility.

In most of our inversions, minimum misfit value remains quite high, which could lead to one of two conclusions that (a) the classical formulation of the SPL used here is not sufficiently complex to reproduce a steady-state landscape or (b) that geomorphic steady-state does not exist or does not apply to the Whataroa catchment. Further investigation is required to determine if introducing in the SPL spatial variations in K related to lithology or precipitation patterns, a better parameterization of channel width or the effect of sediment load on the incision power of a stream would lead to a substantial reduction in misfit.

To progress in testing and improving stream incision laws also requires that we go beyond fitting topographic data and introduce in our inversions observational evidence on the temporal evolution of a stream profile. This include a broad range of thermochronometric tools as well as exposure dating techniques. Sediment provenance data is another important tool that should provide independent information to constrain the SPL (or other potential parameterizations).

7 Conclusions and perspectives

We have presented here a novel approach to constrain the coefficients of the Stream Power Law parameters that combines a very efficient Surface Processes Model (FastScape) and an inversion method (the Neighbourhood Algorithm). The inversion is constrained by a misfit function that compares a reference or observed topography with that predicted by the SPM under the assumption of geomorphic steady-state. Using the method on synthetic landscapes we have demonstrated its potential by an in-depth analysis of the resulting misfit function that is dependent on the number of degrees of freedom (or model parameters) in the inversion procedure. We proved that the method is accurate and efficient to retrieve the ratio between m and n , the two exponents in the SPL formulation, that strongly controls the concavity of river profiles.

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We applied the method to a natural landscape from the South Island of New Zealand where geomorphic steady-state is likely to be achieved due to the present-day very high tectonically-driven uplift rates. In this case, we show that the ratio m/n can be constrained but the estimate we obtain is close to the upper bound of commonly “accepted” values, suggesting that the region may be subject to substantial spatial variations in uplift rate. We also show that the value of none of the SPL coefficients can be retrieved with confidence due to the presence of a spurious solution corresponding to $m = n = 0$ and $K = U$.

We also performed an inversion in which uplift rate was allowed to vary spatially around a fixed mean value, that is relatively well constrained in NZ through the interpretation of many thermochronological datasets. The results show that the preferred solution (i.e. the one that minimizes the misfit between observed and predicted elevation) implies a decrease in uplift rate towards the Alpine Fault, which is consistent with a recent study demonstrating that the strong gradient in deformation east of the Alpine Fault indicates that uplift rate must increase with distance from the Alpine Fault (Braun et al., 2010).

We also conclude that although promising, the method we have developed needs to be improved to include transient effects, other observational constraints on the temporal evolution of landscapes and the spatial distribution of erosion rate in and out of the channels, which will also require to modify the misfit function.

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Table 1. Parametrization of the different runs.

RUN	m	n	$K (m^{1-2\text{myr}^{-1}})$	$U(\text{myr}^{-1})$	N_{total}	N_{init}	N_{it}
Synthetic cases:							
Reference Model	0.4	1	10^{-5}	0.0005			
nm	0.1/2	0.2/4	fixed	fixed	22500	5	10 000
nmk	0.1/2	0.2/4	$10^{-6}/10^{-4}$	fixed	90000	10	30 000
$unmk$	0.1/2	0.2/4	$10^{-6}/10^{-4}$	0.0003/0.0008	90000	10	30 000
Whataroa case:							
nmk	0.1/2	0.2/4	$10^{-13}/10^{-4}$	fixed	90000	10	30 000
αnmk	0.1/2	0.2/4	$10^{-13}/10^{-4}$	$\alpha : 0/1$	90000	10	30 000

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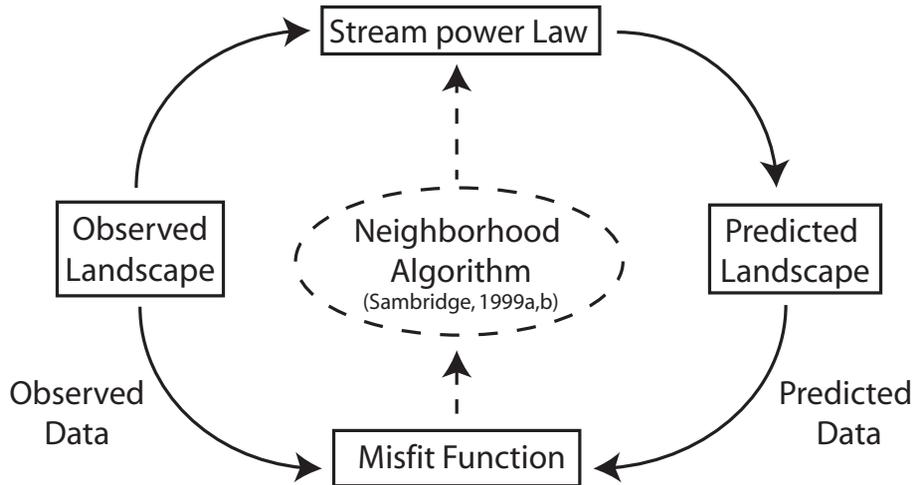


Fig. 1. Scheme for the Inversion. Observed landscape is extracted from a DEM or obtained by running the SPM to steady-state. The predicted landscape is obtained by running the SPL with known parameters (U , K , m and n) values selected by the NA in order to minimize the misfit function obtained by comparing the observed and predicted landscapes.

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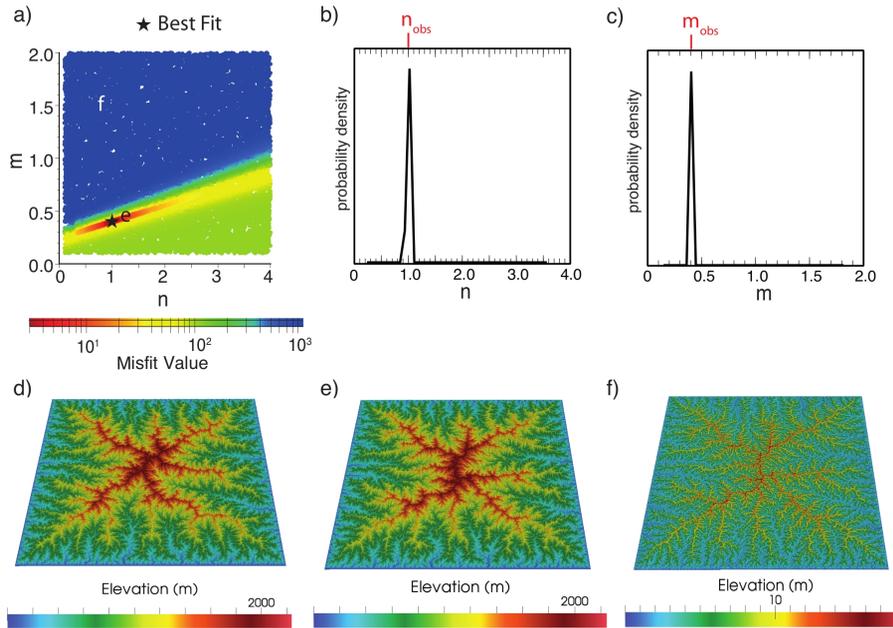


Fig. 2. Results from inversion for the free parameters m and n . **(a)** Scatter plot showing the results from NA sampling stage. The black star is the best fit model. **(b, c)** PDFs of the two parameters resulting from the NA appraisal stage. **(d)** Reference model topography. **(e)** Topography of the best fit model. **(f)** Topography of a high misfit value model.

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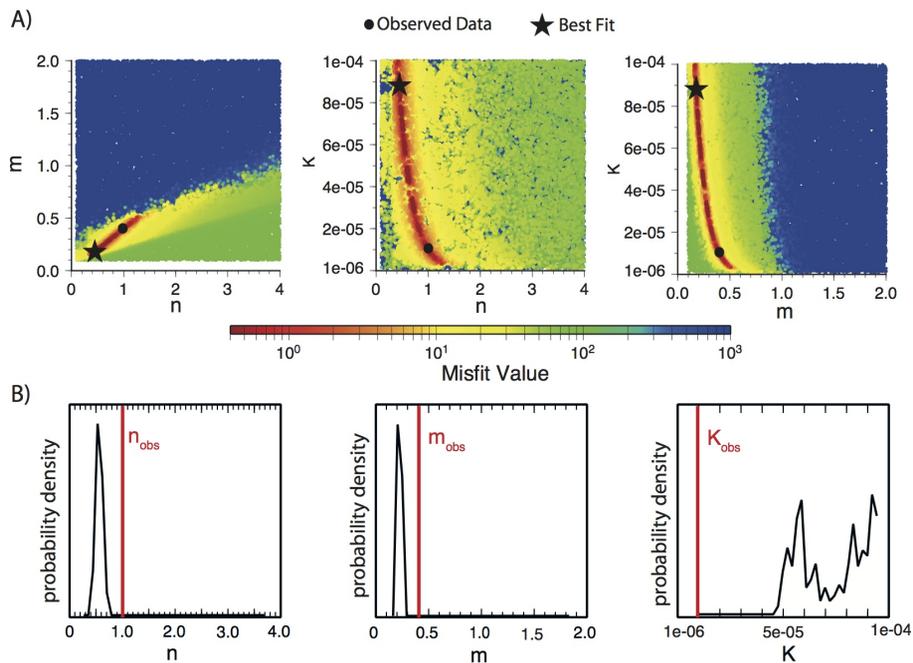


Fig. 3. Results from inversion for the free parameters m , n and K . **(A)** Scatter plots showing the results from NA sampling stage. **(B)** PDFs of the three parameters resulting from the appraisal stage of NA.

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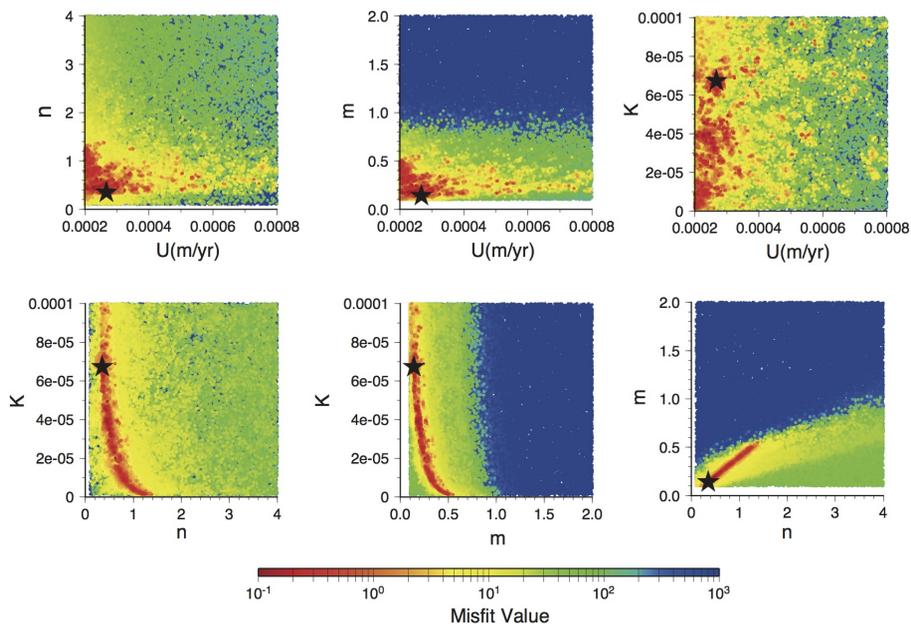


Fig. 4. Results from inversion for the free parameters U , K , m and n . Scatter plots showing the results from NA sampling stage.

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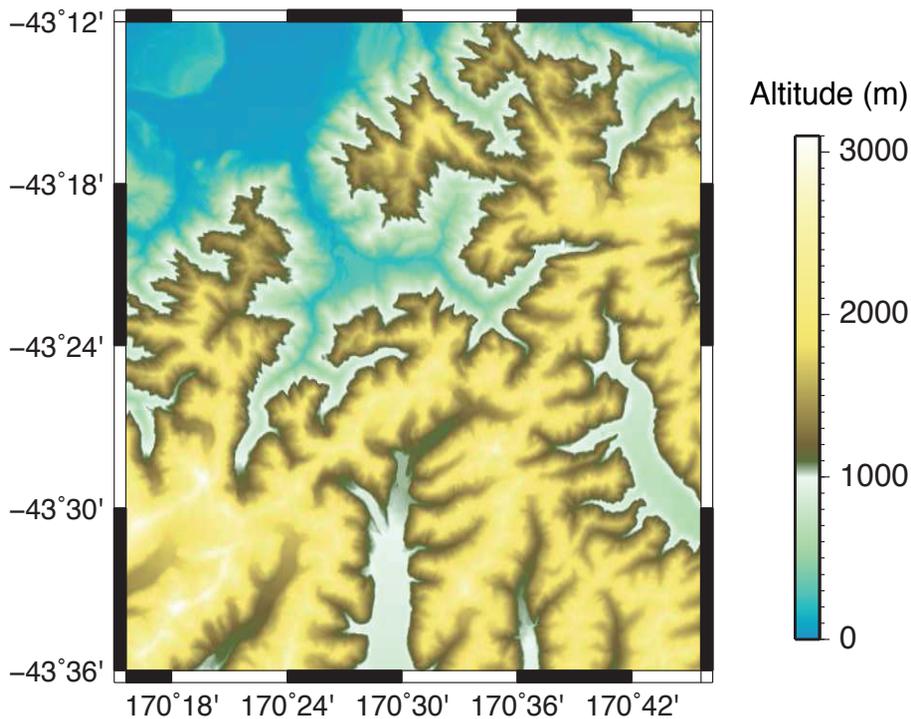


Fig. 5. Whataroa catchment in the Southern Alps, New Zealand.

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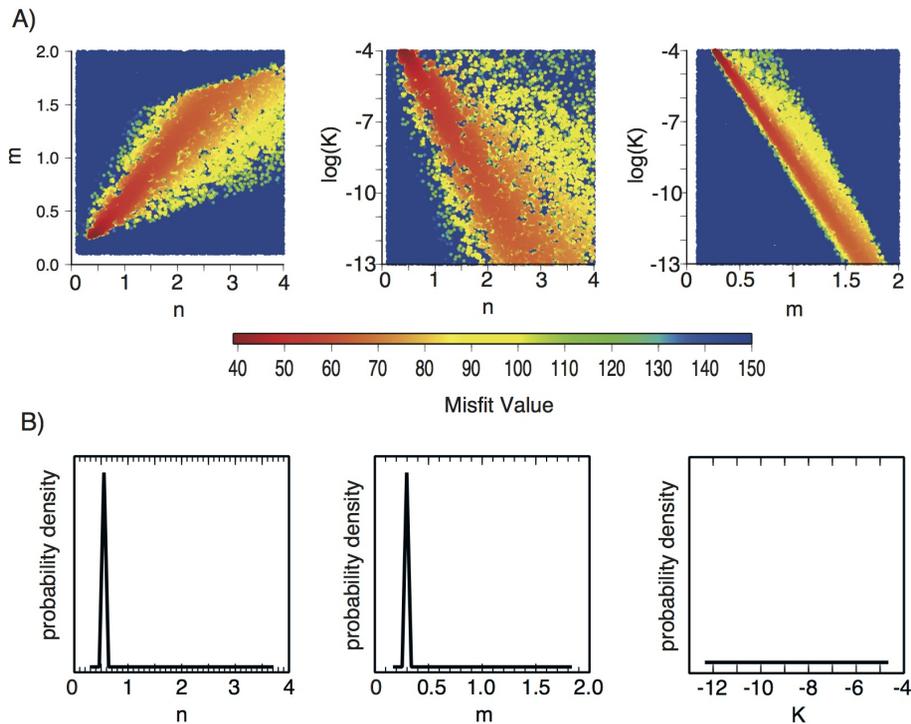


Fig. 6. Results from inversion for the free parameters K , m and n . **(A)** Scatter plots showing the results from NA sampling stage. **(B)** PDFs of the three parameters resulting from the appraisal stage of NA.

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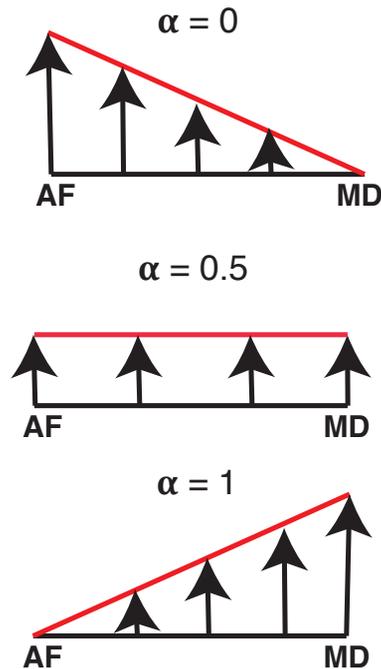


Fig. 7. 3 extreme cases controlled by the value of α . AF: Alpine Fault, MD: main divide.

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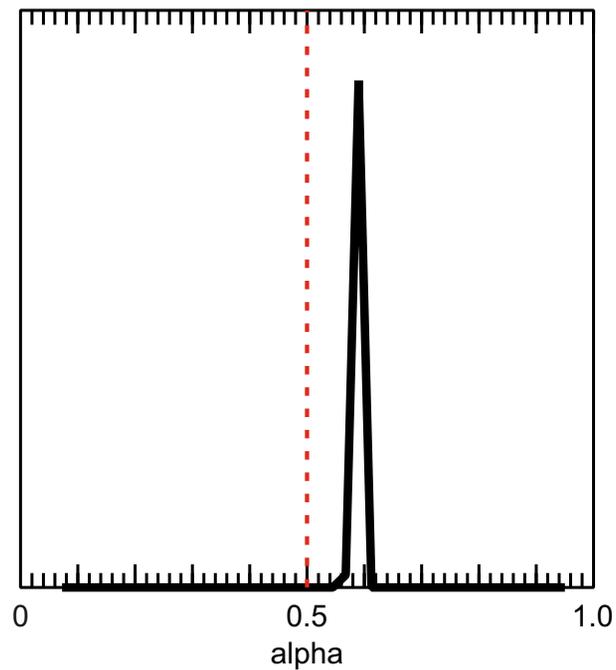
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**Fig. 8.** Results from inversion, PDF of the parameter α .

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