

Interactions between channels and tributary alluvial fans: channel adjustments and sediment-signal propagation

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Supplementary material

This document contains the measured and calculated data used for the analyses reported in the main manuscript. In the following pages the reader finds the raw data of the slope and Q_{s_out} measurements (Table S1 and S2) and of the volumes calculations (Tables S3 to S8). Additional data figures are also provided in support of the information reported in the main manuscript (Table S9 and Figure S1 to S7).

Table S1. Manually measured main channel slope (%) and Qs_out values (ml/s; normalized to Qs_in)

| Run time (min) | MC_NC | | T_NC1 | | T_ISDS | | T_DWIW | | T_NC2 | | T_IWMC | |
|-------------------|-------|--------|-------|--------|--------|--------|--------|--------|-------|--------|--------|--------|
| | Slope | Qs_out | Slope | Qs_out | Slope | Qs_out | Slope | Qs_out | Slope | Qs_out | Slope | Qs_out |
| 0 | 5.3 | | 4.5 | | 4.8 | | 5.0 | | 4.6 | | 5.3 | |
| 10 | 7.3 | 21.3 | 6.8 | 14.0 | 6.8 | 19.8 | 7.4 | 10.1 | 7.1 | 5.9 | 6.9 | 5.6 |
| 20 | 7.2 | 16.7 | 7.0 | 6.9 | 6.8 | 12.4 | 7.6 | 13.4 | 7.3 | 5.9 | 7.0 | 7.2 |
| 30 | 7.3 | 7.0 | 6.9 | 8.6 | 7.1 | 7.3 | 7.5 | 11.1 | 7.2 | 3.2 | 7.1 | 2.9 |
| 40 | 7.4 | 9.7 | 7.0 | 4.6 | 6.9 | 4.2 | 7.9 | 7.9 | 7.3 | 3.6 | 7.4 | 3.9 |
| 50 | 7.6 | 10.1 | 7.1 | 8.9 | 7.3 | 8.6 | 7.8 | 8.5 | 7.4 | 2.9 | 7.5 | 2.6 |
| 60 | 7.5 | 9.8 | 7.3 | 7.2 | 7.0 | 7.9 | 7.8 | 9.2 | 7.4 | 4.0 | 7.5 | 1.8 |
| 70 | 7.6 | 6.4 | 7.3 | 6.2 | 7.3 | 8.1 | 8.0 | 6.3 | 7.7 | 3.4 | 7.4 | 2.0 |
| 80 | 7.7 | 9.1 | 7.4 | 4.6 | 7.4 | 4.9 | 8.0 | 4.7 | 7.9 | 2.3 | 7.6 | 2.0 |
| 90 | 7.8 | 5.1 | 7.4 | | 7.5 | 4.3 | 8.0 | 3.6 | 7.8 | 3.0 | 7.7 | 2.4 |
| 100 | 7.7 | 10.1 | 7.5 | 7.0 | 7.6 | 4.3 | 8.0 | 5.9 | 7.8 | 2.1 | 7.8 | 2.1 |
| 110 | 7.6 | 4.3 | 7.6 | 2.6 | 7.6 | 4.6 | 8.1 | 2.3 | 7.9 | 4.9 | 7.9 | 1.6 |
| 120 | 7.4 | 9.0 | 7.5 | 2.6 | 7.6 | 8.3 | 8.1 | 4.3 | 7.9 | 4.5 | 7.8 | 1.9 |
| 130 | 7.6 | 3.6 | 7.4 | 9.8 | 7.9 | 3.4 | 8.1 | 3.3 | 8.1 | 4.2 | 7.9 | 4.3 |
| 140 | 7.4 | 3.6 | 7.5 | 2.0 | 8.1 | 4.3 | 8.0 | 2.9 | 8.1 | 4.0 | 7.9 | 3.2 |
| 150 | 7.4 | 4.3 | 7.6 | 5.0 | 7.9 | 2.3 | 7.9 | 3.4 | 8.2 | 1.4 | 8.0 | 2.4 |
| 160 | 7.4 | 5.9 | 7.8 | 4.7 | 8.0 | 4.4 | 8.0 | 3.9 | 8.1 | 2.5 | 8.0 | 2.0 |
| 170 | 7.6 | 8.2 | 7.8 | 2.7 | 7.9 | 2.9 | 8.0 | 4.3 | 8.3 | 2.3 | 8.2 | 1.3 |
| 180 | 7.4 | 4.0 | 7.8 | | 7.9 | 4.6 | 8.0 | 3.2 | 8.2 | 2.9 | 8.1 | 2.7 |
| 190 | 7.4 | 4.2 | 7.6 | 5.1 | 7.9 | 1.7 | 8.0 | 3.0 | 8.1 | 1.9 | 7.5 | 4.7 |
| 200 | 7.5 | 3.9 | 7.5 | 4.3 | 7.9 | 3.7 | 8.0 | 2.2 | 8.3 | 3.2 | 7.4 | 3.9 |
| 210 | 7.3 | 3.4 | 7.3 | 7.3 | 7.6 | 4.9 | 8.0 | 2.4 | 8.3 | 1.3 | 7.3 | 3.7 |
| 220 | 7.2 | 2.9 | 7.6 | 3.2 | 7.6 | 2.9 | 8.0 | 3.6 | 8.2 | 2.9 | 7.3 | 5.7 |
| 230 | 7.3 | 3.6 | 7.5 | 2.4 | 7.6 | 6.0 | 7.9 | 3.2 | 8.3 | 1.9 | 7.1 | 2.9 |
| 240 | 7.1 | 2.9 | 7.6 | 4.1 | 7.6 | 5.7 | 7.6 | 2.8 | 8.3 | 2.6 | 6.9 | 6.4 |
| 250 | 7.1 | 2.3 | 7.5 | 3.0 | 7.8 | 2.6 | 7.6 | 3.7 | 8.3 | 2.4 | 7.1 | 2.6 |
| 260 | 7.1 | 3.6 | 7.6 | 6.3 | 7.5 | 3.3 | 7.8 | 3.2 | 8.4 | 1.9 | 7.0 | 2.5 |
| 270 | 7.1 | 2.6 | 7.4 | 2.9 | 7.6 | 2.0 | 7.6 | 3.7 | 8.3 | 1.3 | 7.0 | 3.4 |
| 280 | 7.2 | 5.6 | 7.5 | 2.9 | 7.8 | 2.6 | 7.6 | 3.2 | 8.4 | 1.7 | 7.1 | 3.2 |
| 290 | 7.3 | 3.3 | 7.6 | 4.9 | 7.8 | 3.0 | 7.4 | 4.0 | 8.5 | 3.0 | 7.0 | 2.6 |
| 300 | 7.0 | 5.4 | 7.5 | | 7.6 | 3.5 | 7.3 | 5.7 | 8.4 | 2.7 | 6.9 | 2.0 |
| 310 | 7.1 | 2.8 | 7.5 | 2.9 | 7.4 | 1.2 | 7.4 | 1.8 | 8.4 | 1.3 | 6.9 | 3.7 |
| 320 | 7.1 | 5.2 | 7.5 | 2.6 | 7.6 | 1.8 | 7.1 | 3.3 | 8.6 | 1.9 | 7.0 | 3.4 |
| 330 | 7.0 | 4.0 | 7.5 | 2.6 | 7.6 | 2.2 | 7.0 | 1.6 | 8.5 | 0.9 | 6.8 | 2.3 |
| 340 | 7.1 | 3.0 | 7.4 | 5.9 | 7.3 | 2.4 | 7.3 | 1.6 | 8.6 | 1.7 | 6.9 | 3.3 |
| 350 | 7.1 | 4.4 | 7.4 | 3.6 | 7.3 | 1.5 | 7.1 | 1.4 | 8.6 | 1.3 | 6.9 | 2.2 |
| 360 | 7.1 | 3.6 | 7.4 | 3.9 | 7.4 | 2.8 | 7.2 | 1.9 | 8.5 | 2.7 | 6.8 | 2.2 |
| 370 | 7.0 | 2.0 | 7.4 | 3.9 | 7.5 | 1.7 | 7.3 | 1.7 | 8.6 | 1.6 | 6.9 | 3.3 |
| 380 | 7.1 | 3.1 | 7.1 | 2.5 | 7.5 | 1.1 | 7.3 | 1.7 | 8.6 | 0.9 | 6.9 | 2.8 |
| 390 | 6.9 | 4.7 | 7.4 | 5.3 | 7.8 | 0.9 | 7.2 | 2.0 | 8.5 | 2.0 | 6.8 | 2.2 |
| 400 | 7.1 | 2.3 | 7.3 | 1.7 | 7.6 | 1.2 | 7.4 | 3.7 | 8.6 | 2.2 | 6.8 | 2.7 |
| 410 | 7.1 | 2.3 | 7.3 | 3.4 | 7.5 | 1.6 | 7.1 | 5.2 | 8.7 | 2.6 | 7.0 | 4.9 |
| 420 | 7.0 | 3.2 | 7.4 | 2.0 | 7.4 | | 7.3 | 2.3 | 8.4 | 2.1 | 7.0 | 2.1 |
| 430 | 6.9 | 2.8 | 7.1 | 1.8 | 7.3 | 1.2 | 7.3 | 3.4 | 8.6 | 2.3 | 7.0 | 3.4 |
| 440 | 7.0 | 3.6 | 7.3 | 1.5 | 7.3 | 0.5 | 7.1 | 4.2 | 8.6 | 1.4 | 6.9 | 4.9 |
| 450 | 6.9 | 4.2 | 7.3 | 1.5 | 7.3 | 2.4 | 7.3 | 3.2 | 8.6 | 1.0 | 6.9 | 2.3 |
| 460 | 6.9 | 1.4 | 7.3 | 1.3 | 7.1 | 1.9 | 7.3 | 3.4 | 8.6 | 1.5 | 6.9 | 5.2 |
| 470 | 7.1 | 2.8 | 7.1 | 1.7 | 7.1 | 2.3 | 7.5 | 2.6 | 8.5 | 2.7 | 6.6 | 2.5 |
| 480 | 7.0 | 2.4 | 7.1 | 1.9 | 7.3 | 1.7 | 7.5 | 1.9 | 8.4 | 1.8 | 6.8 | 4.3 |
| 490 | 7.0 | 1.9 | 7.3 | 1.9 | 7.4 | 2.5 | 7.3 | 3.9 | | | | |
| 500 | 6.9 | 1.3 | 6.9 | 1.6 | 7.6 | 1.4 | 7.1 | 4.7 | | | | |
| 510 | 6.9 | 3.1 | 6.8 | 1.6 | 7.4 | 1.7 | 7.2 | 2.5 | | | | |
| 520 | 6.9 | 2.0 | 6.9 | 1.6 | 7.3 | 1.1 | 7.3 | 1.6 | | | | |
| 530 | 6.9 | 1.7 | 6.8 | 1.4 | 7.3 | 4.5 | 7.4 | 2.2 | | | | |

| | | | | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|--|--|--|--|
| 540 | 7.0 | 1.4 | 6.6 | 2.2 | 7.1 | 2.6 | 7.3 | 2.7 | | | | |
| 550 | 6.8 | 2.0 | 6.8 | 1.7 | 7.1 | 1.1 | 7.2 | 3.0 | | | | |
| 560 | 6.9 | 2.3 | 6.8 | 1.4 | 7.0 | 3.9 | 7.3 | 4.2 | | | | |
| 570 | 6.9 | 2.9 | 6.5 | 1.3 | 7.1 | 6.3 | 7.4 | | | | | |
| 580 | 7.0 | 2.1 | 6.5 | 1.8 | 7.1 | 2.1 | 7.3 | 2.2 | | | | |
| 590 | 6.9 | 2.2 | 6.6 | 1.3 | 7.4 | 2.1 | 7.4 | 2.0 | | | | |
| 600 | 6.8 | 1.9 | 6.5 | 0.0 | 7.3 | 2.6 | 7.3 | | | | | |
| 610 | 7.0 | 4.7 | | | 7.3 | 2.6 | 7.3 | 2.1 | | | | |
| 620 | 7.0 | 1.4 | | | 7.3 | 2.2 | 7.4 | 2.7 | | | | |
| 630 | 6.8 | 1.6 | | | 7.3 | 2.4 | 7.4 | 2.3 | | | | |
| 640 | 6.8 | 2.9 | | | 7.3 | 3.0 | 7.3 | 1.7 | | | | |
| 650 | 6.9 | 2.3 | | | 7.1 | 1.4 | 7.3 | 1.8 | | | | |
| 660 | 6.8 | 2.2 | | | 7.2 | 2.6 | 7.2 | 1.7 | | | | |
| 670 | 7.1 | 1.9 | | | 7.3 | 0.9 | | | | | | |
| 680 | 6.7 | 1.2 | | | 7.3 | 1.7 | | | | | | |
| 690 | 6.7 | 2.5 | | | 7.1 | 2.4 | | | | | | |
| 700 | | | | | 7.1 | 1.8 | | | | | | |
| 710 | | | | | 7.1 | 1.4 | | | | | | |
| 720 | | | | | 7.3 | 1.2 | | | | | | |

Table S2. Calculated slope (%) for the tributary channel (using DEMs).

| Runtime (min) | T_NC1 | T_ISDS | T_DWIW | T_NC2 | T_IWMC |
|---------------|-------|--------|--------|-------|--------|
| 30 | 11.0 | 11.2 | 9.4 | 12.8 | 10.6 |
| 60 | 8.6 | 9.9 | 12.0 | 12.5 | 12.7 |
| 90 | 9.6 | 11.7 | 10.9 | 12.6 | 12.3 |
| 120 | 9.6 | 10.9 | 11.1 | 13.2 | 13.2 |
| 150 | 9.7 | 11.7 | 10.5 | 11.7 | 12.4 |
| 180 | 6.4 | 10.3 | 11.3 | 11.5 | 12.0 |
| 210 | 8.2 | 9.0 | 10.7 | 11.1 | 11.9 |
| 240 | 7.4 | 9.1 | 10.4 | 12.0 | 13.0 |
| 270 | 10.0 | 8.0 | 11.0 | 10.9 | 13.5 |
| 300 | 9.1 | 8.2 | 9.7 | 13.1 | 12.5 |
| 330 | 11.4 | 8.3 | 11.5 | 10.3 | 12.2 |
| 360 | 11.8 | 11.0 | 11.1 | 11.4 | 11.4 |
| 390 | 10.5 | 11.4 | 13.0 | 11.4 | 11.7 |
| 420 | 8.6 | 11.9 | 11.2 | 12.1 | 12.0 |
| 450 | 9.3 | 11.9 | 10.4 | 10.2 | 13.2 |
| 480 | 8.7 | 10.2 | 9.1 | 11.1 | 12.0 |
| 510 | 8.8 | 12.6 | 10.4 | | |
| 540 | 10.8 | 12.5 | 9.8 | | |
| 570 | 8.9 | 9.4 | 9.2 | | |
| 600 | 10.5 | 10.8 | 9.0 | | |
| 630 | | 10.2 | 10.1 | | |
| 660 | | 10.1 | 9.8 | | |
| 690 | | 9.6 | 10.4 | | |
| 720 | | 9.6 | | | |

Table S3 to S8. Volumes of mobilize sediment for each experiment. Data are divided into upper, middle, and lower sections. The volumes mobilized in the whole system is additionally provided at the bottom of each experiment table. The bank contribution in percent is calculated on the total volume of sediment exiting the system.

Table S3. MC_NC experiment. All values are reported in 10^{-3} m^3 over a period of 30 minutes (Run time is in minutes).

| Upper section | | | | | | |
|----------------|------|-----------------------|-------------------|------------------------|-------------------------|-----------------------------|
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 1.490 | -1.010 | 0.000 | 0.000 | 0.000 |
| 90 | 4 | 0.422 | -1.841 | -0.491 | 0.000 | 0.491 |
| 120 | 5 | 0.058 | -1.590 | -0.212 | 0.000 | 0.212 |
| 150 | 6 | 0.173 | -1.986 | -0.024 | 0.000 | 0.024 |
| 180 | 8 | 0.037 | -1.462 | 0.000 | 0.000 | 0.000 |
| 210 | 9 | 0.118 | -0.843 | -0.001 | 0.000 | 0.001 |
| 240 | 10 | 0.107 | -1.768 | 0.000 | 0.000 | 0.000 |
| 270 | 11 | 0.416 | -1.054 | 0.000 | 0.000 | 0.000 |
| 300 | 12 | 0.270 | -0.638 | 0.000 | 0.000 | 0.000 |
| 330 | 13 | 0.473 | -1.032 | -0.018 | 0.000 | 0.018 |
| 360 | 14 | 0.129 | -1.222 | 0.000 | 0.000 | 0.000 |
| 390 | 15 | 0.092 | -1.064 | 0.000 | 0.000 | 0.000 |
| 420 | 16 | 0.212 | -0.836 | -0.033 | 0.000 | 0.032 |
| 450 | 17 | 0.455 | -0.710 | -0.126 | 0.001 | 0.125 |
| 480 | 19 | 0.279 | -0.521 | -0.055 | 0.001 | 0.054 |
| 510 | 20 | 0.110 | -0.558 | -0.160 | 0.002 | 0.158 |
| 540 | 21 | 0.332 | -0.518 | -0.224 | 0.000 | 0.224 |
| 570 | 22 | 0.096 | -0.727 | -0.313 | 0.000 | 0.313 |
| 600 | 23 | 0.512 | -0.400 | -0.045 | 0.002 | 0.043 |
| 630 | 24 | 0.433 | -0.429 | -0.124 | 0.085 | 0.039 |
| 660 | 25 | 0.040 | -1.500 | -0.201 | 0.000 | 0.201 |
| 690 | 26 | 0.168 | -0.680 | -0.006 | 0.001 | 0.005 |
| Middle section | | | | | | |
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 0.002 | -3.665 | -2.831 | 0.000 | 2.831 |
| 90 | 4 | 0.041 | -2.736 | -1.730 | 0.000 | 1.730 |
| 120 | 5 | 0.367 | -0.927 | -2.467 | 0.000 | 2.467 |
| 150 | 6 | 0.077 | -1.875 | -1.201 | 0.001 | 1.200 |
| 180 | 8 | 0.257 | -1.394 | -0.560 | 0.002 | 0.558 |
| 210 | 9 | 0.005 | -2.815 | -0.120 | 0.002 | 0.118 |
| 240 | 10 | 0.982 | -0.729 | -1.804 | 0.011 | 1.793 |
| 270 | 11 | 0.849 | -0.840 | -1.363 | 0.006 | 1.357 |
| 300 | 12 | 0.125 | -1.919 | -1.342 | 0.109 | 1.233 |
| 330 | 13 | 0.300 | -1.869 | -0.917 | 0.007 | 0.909 |
| 360 | 14 | 0.151 | -1.641 | -0.418 | 0.094 | 0.324 |
| 390 | 15 | 0.672 | -1.000 | -0.881 | 0.031 | 0.850 |
| 420 | 16 | 0.391 | -1.166 | -0.419 | 0.001 | 0.418 |
| 450 | 17 | 0.280 | -1.006 | -0.404 | 0.101 | 0.302 |
| 480 | 19 | 0.650 | -0.504 | -0.157 | 0.029 | 0.128 |
| 510 | 20 | 0.457 | -0.479 | -0.001 | 0.008 | -0.007 |
| 540 | 21 | 0.442 | -0.649 | -0.533 | 0.004 | 0.529 |
| 570 | 22 | 0.345 | -1.208 | -0.279 | 0.105 | 0.174 |
| 600 | 23 | 0.963 | -0.955 | -0.958 | 0.001 | 0.957 |
| 630 | 24 | 0.471 | -1.615 | -1.104 | 0.345 | 0.759 |
| 660 | 25 | 0.964 | -0.947 | -0.222 | 0.078 | 0.144 |
| 690 | 26 | 0.714 | -0.959 | -1.133 | 0.278 | 0.856 |

| Lower section | | | | | | |
|----------------------|-------------|--|--------------------------------------|--|---|---|
| Run time | DE M | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 0.093 | -5.770 | -5.938 | 0.078 | 5.860 |
| 90 | 4 | 0.039 | -3.997 | -1.633 | 0.003 | 1.630 |
| 120 | 5 | 0.382 | -1.800 | -1.847 | 0.002 | 1.845 |
| 150 | 6 | 0.684 | -1.522 | -2.689 | 0.006 | 2.682 |
| 180 | 8 | 0.637 | -1.557 | -0.238 | 0.001 | 0.237 |
| 210 | 9 | 0.384 | -2.268 | -1.149 | 0.041 | 1.108 |
| 240 | 10 | 1.032 | -1.117 | -1.457 | 0.048 | 1.409 |
| 270 | 11 | 1.007 | -2.156 | -3.332 | 0.584 | 2.749 |
| 300 | 12 | 1.162 | -1.209 | -1.400 | 0.190 | 1.210 |
| 330 | 13 | 0.690 | -1.655 | -0.317 | 0.006 | 0.311 |
| 360 | 14 | 0.467 | -2.126 | -0.244 | 0.002 | 0.242 |
| 390 | 15 | 1.069 | -1.521 | -1.018 | 0.317 | 0.701 |
| 420 | 16 | 1.041 | -1.421 | -0.560 | 0.054 | 0.506 |
| 450 | 17 | 0.565 | -1.373 | -1.072 | 0.025 | 1.047 |
| 480 | 19 | 0.523 | -1.200 | -0.001 | 0.001 | 0.001 |
| 510 | 20 | 1.084 | -1.644 | -1.654 | 0.001 | 1.653 |
| 540 | 21 | 1.202 | -1.265 | -0.691 | 0.040 | 0.651 |
| 570 | 22 | 0.961 | -1.241 | -0.360 | 0.007 | 0.353 |
| 600 | 23 | 0.616 | -1.278 | -0.142 | 0.000 | 0.142 |
| 630 | 24 | 0.730 | -0.845 | -0.188 | 0.004 | 0.184 |
| 660 | 25 | 0.747 | -1.146 | -0.389 | 0.022 | 0.366 |
| 690 | 26 | 0.547 | -1.083 | -0.553 | 0.026 | 0.527 |

Whole system

| Run time | DEM | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution | |
|-----------------|------------|--|--------------------------------------|--|---|---------------------------|------------|
| | | | | | | (V_b) | (%) |
| 60 | 3 | 1.696 | -10.882 | -9.342 | 0.078 | 9.263 | 50.2 |
| 90 | 4 | 0.542 | -8.893 | -3.871 | 0.007 | 3.864 | 31.6 |
| 120 | 5 | 0.860 | -4.679 | -4.821 | 0.013 | 4.808 | 55.7 |
| 150 | 6 | 1.092 | -5.579 | -4.113 | 0.007 | 4.105 | 47.8 |
| 180 | 8 | 1.057 | -4.601 | -0.902 | 0.003 | 0.899 | 20.2 |
| 210 | 9 | 0.665 | -6.133 | -1.414 | 0.049 | 1.365 | 20.0 |
| 240 | 10 | 2.136 | -3.888 | -3.288 | 0.059 | 3.228 | 64.8 |
| 270 | 11 | 2.308 | -4.242 | -4.697 | 0.590 | 4.107 | 68.0 |
| 300 | 12 | 1.815 | -3.859 | -3.269 | 0.299 | 2.971 | 59.2 |
| 330 | 13 | 1.506 | -4.774 | -1.270 | 0.014 | 1.256 | 27.8 |
| 360 | 14 | 0.763 | -5.297 | -0.663 | 0.097 | 0.566 | 11.1 |
| 390 | 15 | 1.946 | -3.793 | -1.900 | 0.349 | 1.550 | 45.6 |
| 420 | 16 | 1.816 | -3.508 | -1.012 | 0.056 | 0.956 | 36.1 |
| 450 | 17 | 1.350 | -3.243 | -1.607 | 0.128 | 1.479 | 43.9 |
| 480 | 19 | 1.501 | -2.403 | -0.213 | 0.031 | 0.182 | 16.8 |
| 510 | 20 | 1.814 | -2.819 | -1.814 | 0.011 | 1.804 | 64.2 |
| 540 | 21 | 2.106 | -2.546 | -1.452 | 0.044 | 1.408 | 76.2 |
| 570 | 22 | 1.540 | -3.302 | -0.953 | 0.112 | 0.841 | 32.3 |
| 600 | 23 | 2.155 | -2.754 | -1.145 | 0.003 | 1.142 | 65.6 |
| 630 | 24 | 1.729 | -3.008 | -1.416 | 0.437 | 0.979 | 43.4 |
| 660 | 25 | 1.893 | -3.755 | -1.112 | 0.118 | 0.994 | 34.8 |
| 690 | 26 | 1.556 | -2.914 | -2.055 | 0.395 | 1.660 | 55.0 |

Table S4. T_NC1 experiment. All values are reported in 10^{-3} m^3 over a period of 30 minutes (Run time is in minutes).

| Upper section | | | | | | |
|-----------------------|-------------|---------------------------------------|-----------------------------------|--|---|---|
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 1.775 | -0.696 | -0.020 | 0.000 | 0.020 |
| 90 | 4 | 1.303 | -0.715 | -0.183 | 0.000 | 0.183 |
| 120 | 5 | 0.691 | -0.869 | -0.496 | 0.000 | 0.496 |
| 150 | 6 | 0.386 | -1.060 | -0.706 | 0.000 | 0.706 |
| 180 | 7 | 0.204 | -0.993 | -0.517 | 0.003 | 0.514 |
| 210 | 8 | 0.162 | -2.010 | -0.696 | 0.000 | 0.695 |
| 240 | 9 | 0.282 | -1.653 | -0.400 | 0.000 | 0.400 |
| 270 | 10 | 0.247 | -1.301 | -0.436 | 0.000 | 0.436 |
| 300 | 11 | 0.175 | -0.521 | -1.426 | 0.000 | 1.426 |
| 330 | 12 | 0.221 | -1.362 | -1.407 | 0.001 | 1.407 |
| 360 | 14 | 0.424 | -1.809 | -2.210 | 0.002 | 2.208 |
| 390 | 15 | 0.333 | -2.045 | -0.283 | 0.002 | 0.281 |
| 420 | 16 | 0.240 | -2.095 | -0.137 | 0.004 | 0.134 |
| 450 | 17 | 0.037 | -2.155 | -0.013 | 0.019 | -0.005 |
| 480 | 18 | 0.176 | -2.328 | -0.853 | 0.123 | 0.729 |
| 510 | 19 | 0.293 | -2.059 | -0.303 | 0.005 | 0.299 |
| 540 | 20 | 0.106 | -2.333 | -0.003 | 0.000 | 0.003 |
| 570 | 21 | 0.226 | -1.495 | -0.002 | 0.001 | 0.001 |
| 600 | 22 | 0.122 | -1.399 | -0.080 | 0.002 | 0.078 |
| Middle section | | | | | | |
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 0.210 | -3.311 | -12.683 | 0.000 | 12.683 |
| 90 | 4 | 0.208 | -3.819 | -3.665 | 0.000 | 3.665 |
| 120 | 5 | 0.236 | -3.086 | -2.456 | 0.002 | 2.454 |
| 150 | 6 | 0.360 | -2.600 | -1.102 | 0.009 | 1.093 |
| 180 | 7 | 0.431 | -2.372 | -1.178 | 0.269 | 0.909 |
| 210 | 8 | 0.288 | -5.014 | -0.860 | 0.065 | 0.795 |
| 240 | 9 | 0.242 | -2.959 | -1.455 | 0.005 | 1.451 |
| 270 | 10 | 0.470 | -4.149 | -1.629 | 0.002 | 1.626 |
| 300 | 11 | 0.406 | -2.279 | -0.372 | 0.004 | 0.367 |
| 330 | 12 | 0.166 | -3.429 | -2.012 | 0.002 | 2.010 |
| 360 | 14 | 1.205 | -2.012 | -1.526 | 0.004 | 1.522 |
| 390 | 15 | 0.229 | -4.455 | -1.599 | 0.003 | 1.596 |
| 420 | 16 | 0.158 | -3.501 | -0.350 | 0.002 | 0.348 |
| 450 | 17 | 0.977 | -2.187 | -0.579 | 0.005 | 0.573 |
| 480 | 18 | 0.490 | -3.108 | -0.573 | 0.003 | 0.570 |
| 510 | 19 | 0.809 | -1.400 | -0.270 | 0.003 | 0.267 |
| 540 | 20 | 1.487 | -1.411 | -0.672 | 0.050 | 0.623 |
| 570 | 21 | 0.481 | -2.106 | -0.372 | 0.003 | 0.369 |
| 600 | 22 | 0.979 | -1.921 | -0.910 | 0.008 | 0.902 |
| Lower section | | | | | | |
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 0.016 | -5.110 | -12.381 | 0.016 | 12.364 |
| 90 | 4 | 0.990 | -1.676 | -15.225 | 0.012 | 15.213 |
| 120 | 5 | 0.729 | -1.493 | -16.743 | 0.122 | 16.621 |
| 150 | 6 | 0.252 | -2.875 | -11.660 | 0.238 | 11.422 |
| 180 | 7 | 0.640 | -2.737 | -9.402 | 0.038 | 9.364 |

| | | | | | | |
|-----|----|-------|--------|---------|-------|--------|
| 210 | 8 | 0.231 | -5.420 | -5.717 | 0.041 | 5.676 |
| 240 | 9 | 1.036 | -2.232 | -10.947 | 0.013 | 10.935 |
| 270 | 10 | 1.030 | -3.369 | -4.215 | 0.118 | 4.097 |
| 300 | 11 | 1.563 | -2.496 | -9.180 | 1.431 | 7.749 |
| 330 | 12 | 0.479 | -3.487 | -4.139 | 0.183 | 3.956 |
| 360 | 14 | 1.241 | -1.945 | -4.929 | 3.103 | 1.826 |
| 390 | 15 | 1.139 | -3.009 | -4.460 | 0.048 | 4.413 |
| 420 | 16 | 0.999 | -3.683 | -0.612 | 0.016 | 0.596 |
| 450 | 17 | 1.268 | -2.914 | -0.472 | 0.032 | 0.439 |
| 480 | 18 | 0.929 | -1.683 | -0.016 | 0.026 | -0.010 |
| 510 | 19 | 1.238 | -1.378 | -0.013 | 0.028 | -0.016 |
| 540 | 20 | 1.687 | -1.924 | -0.089 | 0.021 | 0.068 |
| 570 | 21 | 1.092 | -1.472 | -0.014 | 0.026 | -0.013 |
| 600 | 22 | 0.558 | -2.424 | -0.037 | 0.020 | 0.018 |

Whole system

| Run time | DEM | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution | |
|----------|-----|--------------------------|----------------------|------------------------|-------------------------|-------------------|------|
| | | | | | | (V_b) | (%) |
| 60 | 3 | 2.116 | -9.359 | -26.362 | 0.016 | 26.346 | 78.4 |
| 90 | 4 | 2.650 | -6.327 | -20.389 | 0.012 | 20.376 | 84.7 |
| 120 | 5 | 1.846 | -5.586 | -19.792 | 0.126 | 19.665 | 84.0 |
| 150 | 6 | 1.132 | -6.659 | -14.314 | 0.515 | 13.799 | 71.4 |
| 180 | 7 | 1.414 | -6.224 | -11.688 | 0.311 | 11.377 | 70.3 |
| 210 | 8 | 0.719 | -12.803 | -7.295 | 0.108 | 7.187 | 37.3 |
| 240 | 9 | 1.648 | -7.054 | -12.811 | 0.030 | 12.781 | 70.3 |
| 270 | 10 | 1.905 | -9.027 | -6.684 | 0.135 | 6.548 | 47.9 |
| 300 | 11 | 2.179 | -5.586 | -11.238 | 1.437 | 9.801 | 74.2 |
| 330 | 12 | 0.990 | -8.393 | -8.373 | 0.246 | 8.127 | 52.3 |
| 360 | 14 | 2.910 | -6.167 | -10.165 | 3.545 | 6.620 | 67.0 |
| 390 | 15 | 2.134 | -9.640 | -7.248 | 0.054 | 7.194 | 48.9 |
| 420 | 16 | 1.441 | -9.745 | -1.523 | 0.023 | 1.500 | 15.3 |
| 450 | 17 | 2.430 | -7.576 | -1.154 | 0.064 | 1.089 | 17.5 |
| 480 | 18 | 1.713 | -7.309 | -1.884 | 0.157 | 1.727 | 23.6 |
| 510 | 19 | 2.420 | -5.252 | -0.711 | 0.040 | 0.672 | 19.2 |
| 540 | 20 | 3.397 | -5.965 | -0.766 | 0.073 | 0.694 | 21.3 |
| 570 | 21 | 1.971 | -5.141 | -0.389 | 0.032 | 0.357 | 10.1 |
| 600 | 22 | 1.721 | -5.879 | -1.030 | 0.031 | 0.999 | 19.4 |

Table S5. T_ISDS experiment. All values are reported in 10^{-3} m^3 over a period of 30 minutes (Run time is in minutes).

| Upper section | | | | | | | |
|---------------|------|--------------------------|----------------------|------------------------|-------------------------|-----------------------------|--|
| Run time | DE M | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) | |
| 60 | 3 | 1.733 | -0.651 | -0.024 | 0.000 | 0.024 | |
| 90 | 4 | 1.656 | -0.833 | -0.085 | 0.000 | 0.085 | |
| 120 | 5 | 1.032 | -0.871 | -0.420 | 0.000 | 0.420 | |
| 150 | 6 | 0.779 | -1.094 | -1.308 | 0.000 | 1.308 | |
| 180 | 7 | 0.817 | -0.813 | -1.170 | 0.000 | 1.170 | |
| 210 | 9 | 0.272 | -2.324 | -0.935 | 0.001 | 0.933 | |
| 240 | 11 | 0.522 | -1.055 | -0.878 | 0.006 | 0.872 | |
| 270 | 12 | 0.495 | -0.692 | -0.521 | 0.001 | 0.521 | |
| 300 | 13 | 0.337 | -1.154 | -0.818 | 0.003 | 0.815 | |
| 330 | 14 | 0.125 | -1.516 | -2.384 | 0.008 | 2.376 | |
| 360 | 15 | 0.022 | -1.806 | -0.187 | 0.001 | 0.186 | |

| | | | | | | |
|-----|----|-------|--------|--------|-------|-------|
| 390 | 16 | 0.097 | -1.319 | -0.052 | 0.035 | 0.017 |
| 420 | 17 | 0.186 | -0.552 | -0.562 | 0.001 | 0.561 |
| 450 | 19 | 0.458 | -0.814 | -0.583 | 0.006 | 0.577 |
| 480 | 20 | 0.572 | -1.226 | -0.523 | 0.030 | 0.493 |
| 510 | 21 | 0.246 | -2.032 | -1.472 | 0.271 | 1.201 |
| 540 | 22 | 0.745 | -1.731 | -1.299 | 0.055 | 1.244 |
| 570 | 23 | 0.471 | -0.977 | -1.172 | 0.001 | 1.171 |
| 600 | 24 | 0.836 | -1.499 | -0.311 | 0.078 | 0.232 |
| 630 | 25 | 0.304 | -0.665 | -0.362 | 0.018 | 0.345 |
| 660 | 26 | 0.408 | -1.371 | -0.256 | 0.001 | 0.255 |
| 690 | 27 | 0.734 | -1.060 | -0.027 | 0.005 | 0.022 |
| 720 | 28 | 0.316 | -0.659 | -0.883 | 0.301 | 0.582 |

Middle section

| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
|----------|------|-----------------------|-------------------|------------------------|-------------------------|-----------------------------|
| 60 | 3 | 1.558 | -1.489 | -13.991 | 0.000 | 13.991 |
| 90 | 4 | 0.168 | -5.316 | -7.828 | 0.027 | 7.802 |
| 120 | 5 | 0.239 | -2.597 | -4.204 | 0.001 | 4.203 |
| 150 | 6 | 0.961 | -1.566 | -4.134 | 0.011 | 4.123 |
| 180 | 7 | 0.561 | -4.485 | -1.829 | 0.278 | 1.551 |
| 210 | 9 | 1.462 | -3.040 | -2.131 | 0.018 | 2.113 |
| 240 | 11 | 1.708 | -2.441 | -0.496 | 0.278 | 0.218 |
| 270 | 12 | 0.583 | -3.631 | -0.980 | 0.504 | 0.476 |
| 300 | 13 | 0.545 | -3.996 | -1.543 | 0.019 | 1.524 |
| 330 | 14 | 1.169 | -2.262 | -0.717 | 0.048 | 0.669 |
| 360 | 15 | 1.696 | -3.458 | -0.038 | 0.003 | 0.035 |
| 390 | 16 | 3.359 | -1.155 | -0.674 | 0.002 | 0.672 |
| 420 | 17 | 3.106 | -1.109 | -0.707 | 0.017 | 0.689 |
| 450 | 19 | 3.016 | -1.115 | -1.412 | 0.747 | 0.665 |
| 480 | 20 | 2.730 | -2.975 | -2.446 | 0.239 | 2.208 |
| 510 | 21 | 0.907 | -2.679 | -1.275 | 0.054 | 1.221 |
| 540 | 22 | 1.457 | -2.017 | -0.354 | 0.003 | 0.351 |
| 570 | 23 | 1.847 | -2.646 | -3.076 | 0.744 | 2.332 |
| 600 | 24 | 1.322 | -3.256 | -2.434 | 0.002 | 2.432 |
| 630 | 25 | 0.665 | -2.032 | -2.671 | 0.032 | 2.640 |
| 660 | 26 | 1.383 | -2.565 | -0.560 | 0.017 | 0.544 |
| 690 | 27 | 1.695 | -2.410 | -2.386 | 0.002 | 2.384 |
| 720 | 28 | 1.505 | -4.083 | -0.406 | 0.125 | 0.281 |

Lower section

| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
|----------|------|-----------------------|-------------------|------------------------|-------------------------|-----------------------------|
| 60 | 3 | 1.450 | -1.853 | -16.482 | 0.000 | 16.482 |
| 90 | 4 | 0.516 | -4.613 | -11.784 | 1.038 | 10.746 |
| 120 | 5 | 0.583 | -3.192 | -9.337 | 0.398 | 8.938 |
| 150 | 6 | 1.347 | -2.221 | -8.146 | 0.173 | 7.973 |
| 180 | 7 | 0.657 | -4.074 | -8.794 | 3.060 | 5.734 |
| 210 | 9 | 1.448 | -1.525 | -9.024 | 2.001 | 7.023 |
| 240 | 11 | 2.665 | -1.447 | -12.243 | 0.555 | 11.688 |
| 270 | 12 | 0.532 | -4.877 | -5.675 | 0.007 | 5.668 |
| 300 | 13 | 0.840 | -2.245 | -4.870 | 2.504 | 2.366 |
| 330 | 14 | 1.721 | -1.620 | -6.417 | 0.068 | 6.349 |
| 360 | 15 | 0.659 | -4.546 | -0.907 | 0.012 | 0.894 |
| 390 | 16 | 1.238 | -2.528 | -5.398 | 2.270 | 3.128 |
| 420 | 17 | 1.287 | -2.107 | -2.920 | 0.010 | 2.910 |
| 450 | 19 | 3.109 | -0.640 | -7.602 | 2.356 | 5.247 |
| 480 | 20 | 0.228 | -4.964 | -1.137 | 0.007 | 1.130 |
| 510 | 21 | 1.449 | -2.011 | -2.039 | 0.007 | 2.031 |
| 540 | 22 | 1.778 | -2.432 | -1.376 | 0.014 | 1.363 |
| 570 | 23 | 2.092 | -1.620 | -9.518 | 4.648 | 4.870 |

| | | | | | | |
|-----|----|-------|--------|--------|-------|-------|
| 600 | 24 | 1.876 | -2.551 | -6.514 | 2.266 | 4.248 |
| 630 | 25 | 0.838 | -3.997 | -3.124 | 0.009 | 3.115 |
| 660 | 26 | 1.224 | -2.177 | -2.396 | 0.007 | 2.389 |
| 690 | 27 | 1.993 | -2.429 | -1.264 | 0.010 | 1.254 |
| 720 | 28 | 1.068 | -2.940 | -4.726 | 1.884 | 2.841 |

Whole system

| Run time | DEM | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution | |
|----------|-----|--------------------------|----------------------|------------------------|-------------------------|-------------------|-------|
| | | | | | | (V_b) | (%) |
| 60 | 3 | 4.917 | -4.199 | -31.161 | 0.000 | 31.161 | 102.4 |
| 90 | 4 | 2.486 | -11.114 | -20.217 | 1.065 | 19.153 | 68.9 |
| 120 | 5 | 1.989 | -7.102 | -14.506 | 0.400 | 14.107 | 73.4 |
| 150 | 6 | 3.340 | -4.981 | -14.580 | 0.184 | 14.395 | 89.8 |
| 180 | 7 | 2.110 | -9.482 | -11.797 | 3.342 | 8.455 | 53.4 |
| 210 | 9 | 3.270 | -7.124 | -12.104 | 2.024 | 10.080 | 72.3 |
| 240 | 11 | 5.153 | -5.084 | -14.680 | 1.154 | 13.526 | 100.5 |
| 270 | 12 | 1.856 | -9.462 | -7.576 | 0.514 | 7.062 | 48.1 |
| 300 | 13 | 1.776 | -7.654 | -7.233 | 2.526 | 4.707 | 44.5 |
| 330 | 14 | 3.137 | -5.561 | -9.672 | 0.125 | 9.547 | 79.7 |
| 360 | 15 | 2.393 | -10.168 | -1.154 | 0.017 | 1.137 | 12.8 |
| 390 | 16 | 4.872 | -5.081 | -6.139 | 2.308 | 3.831 | 94.8 |
| 420 | 17 | 4.610 | -4.007 | -4.189 | 0.030 | 4.160 | 117.0 |
| 450 | 19 | 6.939 | -2.698 | -9.695 | 3.109 | 6.586 | 280.9 |
| 480 | 20 | 3.587 | -9.543 | -4.111 | 0.277 | 3.834 | 39.2 |
| 510 | 21 | 2.749 | -6.897 | -4.794 | 0.337 | 4.458 | 51.8 |
| 540 | 22 | 4.023 | -6.526 | -3.310 | 0.073 | 3.237 | 56.4 |
| 570 | 23 | 4.593 | -5.411 | -13.926 | 5.394 | 8.531 | 91.3 |
| 600 | 24 | 4.237 | -7.462 | -9.279 | 2.349 | 6.930 | 68.2 |
| 630 | 25 | 1.889 | -6.840 | -6.168 | 0.059 | 6.108 | 55.2 |
| 660 | 26 | 3.170 | -6.284 | -3.221 | 0.026 | 3.195 | 50.6 |
| 690 | 27 | 4.533 | -6.040 | -4.432 | 0.019 | 4.414 | 74.6 |
| 720 | 28 | 2.975 | -7.930 | -7.218 | 2.530 | 4.688 | 48.6 |

Table S6. T_DWIW experiment. All values are reported in 10^{-3} m^3 over a period of 30 minutes (Run time is in minutes).

| Upper section | | | | | | |
|---------------|------|--------------------------|----------------------|------------------------|-------------------------|-----------------------------|
| Run time | DE M | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 1.048 | -1.367 | -0.012 | 0.000 | 0.012 |
| 90 | 4 | 0.767 | -0.970 | -0.248 | 0.000 | 0.248 |
| 120 | 5 | 0.482 | -0.852 | -0.531 | 0.000 | 0.531 |
| 150 | 6 | 0.195 | -1.327 | -0.369 | 0.000 | 0.369 |
| 180 | 7 | 0.170 | -1.581 | -0.457 | 0.000 | 0.456 |
| 210 | 8 | 0.160 | -1.071 | -0.410 | 0.001 | 0.409 |
| 240 | 9 | 0.541 | -1.699 | -0.242 | 0.000 | 0.242 |
| 270 | 10 | 0.035 | -2.822 | -0.724 | 0.000 | 0.724 |
| 300 | 11 | 0.090 | -1.624 | -0.282 | 0.000 | 0.282 |
| 330 | 13 | 0.036 | -1.879 | -0.102 | 0.001 | 0.102 |
| 360 | 14 | 0.133 | -1.412 | -0.001 | 0.000 | 0.001 |
| 390 | 15 | 0.217 | -0.769 | -0.009 | 0.001 | 0.008 |
| 420 | 16 | 0.600 | -0.550 | -0.369 | 0.003 | 0.366 |
| 450 | 17 | 0.552 | -0.874 | -1.134 | 0.009 | 1.125 |
| 480 | 18 | 0.620 | -1.779 | -0.089 | 0.000 | 0.089 |
| 510 | 19 | 0.077 | -1.221 | -0.083 | 0.000 | 0.083 |

| 540 | 20 | 0.563 | -1.709 | -0.062 | 0.000 | 0.062 |
|-----------------------|------|-----------------------|-------------------|------------------------|-------------------------|-----------------------------|
| 570 | 21 | 0.590 | -1.606 | -0.139 | 0.000 | 0.139 |
| 600 | 22 | 0.732 | -0.602 | -0.446 | 0.000 | 0.446 |
| 630 | 23 | 0.157 | -0.717 | -0.051 | 0.037 | 0.014 |
| 660 | 24 | 0.370 | -0.804 | -0.109 | 0.002 | 0.107 |
| 690 | 25 | 0.052 | -0.675 | -0.071 | 0.000 | 0.071 |
| Middle section | | | | | | |
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 0.635 | -3.560 | -5.567 | 0.000 | 5.567 |
| 90 | 4 | 0.689 | -2.503 | -4.365 | 0.000 | 4.365 |
| 120 | 5 | 0.670 | -1.847 | -6.316 | 0.000 | 6.316 |
| 150 | 6 | 0.467 | -2.802 | -1.306 | 0.161 | 1.144 |
| 180 | 7 | 0.395 | -2.856 | -1.483 | 0.036 | 1.447 |
| 210 | 8 | 0.256 | -3.247 | -0.085 | 0.020 | 0.065 |
| 240 | 9 | 0.721 | -2.469 | -0.665 | 0.018 | 0.647 |
| 270 | 10 | 0.152 | -4.597 | -0.144 | 0.003 | 0.141 |
| 300 | 11 | 0.590 | -4.727 | -0.323 | 0.009 | 0.314 |
| 330 | 13 | 1.280 | -1.845 | -1.464 | 0.125 | 1.339 |
| 360 | 14 | 1.750 | -1.802 | -0.316 | 0.004 | 0.312 |
| 390 | 15 | 0.959 | -0.861 | -0.010 | 0.012 | -0.002 |
| 420 | 16 | 2.326 | -1.442 | -3.676 | 0.141 | 3.535 |
| 450 | 17 | 2.715 | -2.749 | -6.680 | 0.014 | 6.666 |
| 480 | 18 | 0.557 | -3.791 | -1.448 | 0.003 | 1.446 |
| 510 | 19 | 1.019 | -3.313 | -4.474 | 0.022 | 4.451 |
| 540 | 20 | 0.853 | -4.344 | -2.725 | 0.161 | 2.564 |
| 570 | 21 | 1.813 | -3.366 | -5.011 | 1.800 | 3.210 |
| 600 | 22 | 1.095 | -3.360 | -3.059 | 0.003 | 3.056 |
| 630 | 23 | 1.142 | -2.503 | -0.320 | 1.452 | -1.132 |
| 660 | 24 | 2.158 | -2.246 | -7.080 | 1.934 | 5.146 |
| 690 | 25 | 1.103 | -3.125 | -0.284 | 0.016 | 0.268 |
| Lower section | | | | | | |
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 0.129 | -3.326 | -11.569 | 0.020 | 11.549 |
| 90 | 4 | 0.733 | -2.896 | -17.922 | 0.006 | 17.916 |
| 120 | 5 | 0.361 | -4.085 | -4.880 | 0.179 | 4.701 |
| 150 | 6 | 0.300 | -5.205 | -8.545 | 1.094 | 7.451 |
| 180 | 7 | 2.931 | -1.254 | -11.580 | 2.407 | 9.173 |
| 210 | 8 | 0.555 | -2.438 | -9.934 | 0.232 | 9.701 |
| 240 | 9 | 1.106 | -3.421 | -10.849 | 0.187 | 10.662 |
| 270 | 10 | 0.321 | -4.213 | -7.876 | 0.006 | 7.871 |
| 300 | 11 | 0.786 | -3.940 | -10.673 | 4.263 | 6.410 |
| 330 | 13 | 1.119 | -2.037 | -4.303 | 0.037 | 4.266 |
| 360 | 14 | 0.219 | -2.342 | -2.478 | 0.009 | 2.469 |
| 390 | 15 | 0.995 | -1.824 | -3.870 | 0.675 | 3.195 |
| 420 | 16 | 1.087 | -2.459 | -2.617 | 0.002 | 2.614 |
| 450 | 17 | 1.577 | -1.377 | -0.399 | 0.024 | 0.376 |
| 480 | 18 | 0.918 | -2.979 | -1.209 | 0.692 | 0.517 |
| 510 | 19 | 1.411 | -1.463 | -9.344 | 5.989 | 3.355 |
| 540 | 20 | 1.112 | -2.042 | -3.908 | 0.064 | 3.843 |
| 570 | 21 | 1.388 | -2.530 | -2.060 | 0.009 | 2.051 |
| 600 | 22 | 0.927 | -2.390 | -1.937 | 0.009 | 1.927 |
| 630 | 23 | 1.145 | -1.537 | -0.167 | 0.017 | 0.150 |
| 660 | 24 | 0.710 | -2.831 | -0.434 | 0.022 | 0.412 |
| 690 | 25 | 2.649 | -0.838 | -3.556 | 0.109 | 3.447 |

Whole system

| Run time | DEM | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution | |
|----------|-----|-----------------------|-------------------|------------------------|-------------------------|-------------------|------|
| | | | | | | (V_b) | (%) |
| 60 | 3 | 1.990 | -8.639 | -18.494 | 0.021 | 18.474 | 73.5 |
| 90 | 4 | 2.481 | -6.552 | -23.348 | 0.008 | 23.340 | 85.1 |
| 120 | 5 | 1.641 | -7.143 | -12.961 | 0.333 | 12.629 | 69.7 |
| 150 | 6 | 1.007 | -9.587 | -10.979 | 1.260 | 9.719 | 53.1 |
| 180 | 7 | 3.919 | -5.824 | -13.791 | 2.506 | 11.285 | 85.6 |
| 210 | 8 | 1.110 | -7.011 | -10.503 | 0.254 | 10.249 | 63.5 |
| 240 | 9 | 2.445 | -8.028 | -11.814 | 0.207 | 11.607 | 67.5 |
| 270 | 10 | 0.548 | -11.991 | -8.753 | 0.010 | 8.743 | 43.3 |
| 300 | 11 | 1.474 | -10.676 | -11.522 | 4.274 | 7.248 | 44.1 |
| 330 | 13 | 2.487 | -6.004 | -5.895 | 0.164 | 5.731 | 62.0 |
| 360 | 14 | 2.154 | -5.711 | -2.796 | 0.013 | 2.782 | 43.9 |
| 390 | 15 | 2.306 | -3.518 | -3.890 | 0.689 | 3.201 | 72.5 |
| 420 | 16 | 4.162 | -4.620 | -7.167 | 0.262 | 6.905 | 93.8 |
| 450 | 17 | 4.912 | -5.253 | -8.338 | 0.047 | 8.291 | 96.1 |
| 480 | 18 | 2.160 | -8.697 | -3.411 | 1.023 | 2.388 | 26.8 |
| 510 | 19 | 2.658 | -6.110 | -14.341 | 6.013 | 8.328 | 70.7 |
| 540 | 20 | 2.635 | -8.371 | -6.721 | 0.226 | 6.495 | 53.1 |
| 570 | 21 | 3.922 | -7.791 | -7.315 | 1.810 | 5.506 | 58.7 |
| 600 | 22 | 2.932 | -6.544 | -5.442 | 0.013 | 5.429 | 60.0 |
| 630 | 23 | 2.515 | -4.903 | -0.538 | 1.506 | -0.968 | 68.1 |
| 660 | 24 | 3.358 | -5.994 | -7.623 | 1.958 | 5.665 | 68.2 |
| 690 | 25 | 3.866 | -4.765 | -3.911 | 0.125 | 3.786 | 80.8 |

Table S7. T_NC2 experiment. All values are reported in 10^{-3} m^3 over a period of 30 minutes (Run time is in minutes).

| Upper section | | | | | | |
|----------------|------|-----------------------|-------------------|------------------------|-------------------------|-----------------------------|
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 1.998 | -0.480 | 0.000 | 0.000 | 0.000 |
| 90 | 5 | 2.082 | -0.435 | -0.024 | 0.000 | 0.024 |
| 120 | 6 | 1.669 | -0.395 | -0.033 | 0.000 | 0.033 |
| 150 | 7 | 1.324 | -0.470 | -0.006 | 0.000 | 0.006 |
| 180 | 8 | 1.502 | -0.438 | -0.045 | 0.000 | 0.045 |
| 210 | 9 | 1.261 | -0.337 | 0.000 | 0.000 | 0.000 |
| 240 | 10 | 1.546 | -0.618 | -0.198 | 0.000 | 0.198 |
| 270 | 12 | 1.311 | -0.504 | -0.066 | 0.000 | 0.066 |
| 300 | 13 | 1.328 | -0.519 | -0.129 | 0.000 | 0.129 |
| 330 | 14 | 1.140 | -0.452 | -0.162 | 0.000 | 0.162 |
| 360 | 15 | 0.598 | -0.471 | -0.096 | 0.000 | 0.096 |
| 390 | 16 | 0.944 | -0.359 | -0.013 | 0.000 | 0.013 |
| 420 | 17 | 0.985 | -0.248 | 0.000 | 0.000 | 0.000 |
| 450 | 18 | 0.326 | -0.494 | -0.209 | 0.000 | 0.209 |
| 480 | 19 | 1.016 | -0.396 | -0.643 | 0.000 | 0.643 |
| Middle section | | | | | | |
| Run time | DE M | Aggradation (A_v) | Erosion (E_v) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 2.269 | -1.347 | -5.030 | 0.000 | 5.030 |
| 90 | 5 | 1.734 | -1.062 | -4.686 | 0.000 | 4.686 |
| 120 | 6 | 1.645 | -1.771 | -3.598 | 0.000 | 3.598 |
| 150 | 7 | 2.176 | -0.926 | -2.967 | 0.488 | 2.479 |
| 180 | 8 | 1.470 | -1.354 | -2.919 | 0.001 | 2.918 |
| 210 | 9 | 2.533 | -0.723 | -3.288 | 0.083 | 3.205 |
| 240 | 10 | 1.511 | -1.232 | -1.123 | 0.004 | 1.120 |
| 270 | 12 | 2.962 | -1.525 | -1.157 | 0.059 | 1.097 |
| 300 | 13 | 1.066 | -1.610 | -2.216 | 0.037 | 2.179 |

| 330 | 14 | 1.408 | -1.019 | -1.372 | 0.053 | 1.319 |
|----------------------|------|--------------------------|----------------------|------------------------|-------------------------|-----------------------------|
| 360 | 15 | 1.832 | -0.978 | -0.864 | 0.002 | 0.862 |
| 390 | 16 | 1.567 | -1.591 | -2.137 | 0.001 | 2.136 |
| 420 | 17 | 0.715 | -2.778 | -0.980 | 0.015 | 0.965 |
| 450 | 18 | 1.458 | -1.811 | -1.102 | 0.010 | 1.092 |
| 480 | 19 | 1.205 | -1.125 | -0.833 | 0.092 | 0.741 |
| Lower section | | | | | | |
| Run time | DE M | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 0.399 | -1.956 | -5.741 | 0.002 | 5.739 |
| 90 | 5 | 0.330 | -2.057 | -4.739 | 0.033 | 4.706 |
| 120 | 6 | 0.903 | -1.570 | -5.584 | 0.068 | 5.516 |
| 150 | 7 | 0.228 | -3.140 | -2.848 | 0.018 | 2.830 |
| 180 | 8 | 2.177 | -1.495 | -2.978 | 0.004 | 2.974 |
| 210 | 9 | 0.958 | -2.083 | -6.084 | 0.062 | 6.022 |
| 240 | 10 | 1.605 | -1.273 | -3.964 | 0.003 | 3.961 |
| 270 | 12 | 2.603 | -1.233 | -3.834 | 0.158 | 3.676 |
| 300 | 13 | 1.131 | -1.953 | -1.865 | 0.020 | 1.845 |
| 330 | 14 | 0.858 | -2.271 | -5.217 | 0.757 | 4.460 |
| 360 | 15 | 1.154 | -1.566 | -2.897 | 0.025 | 2.872 |
| 390 | 16 | 1.364 | -1.261 | -5.408 | 2.125 | 3.284 |
| 420 | 17 | 0.532 | -2.196 | -1.780 | 0.078 | 1.702 |
| 450 | 18 | 1.515 | -1.301 | -5.371 | 0.896 | 4.475 |
| 480 | 19 | 1.848 | -1.890 | -5.235 | 0.221 | 5.013 |

Whole system

| Run time | DEM | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution | |
|----------|-----|--------------------------|----------------------|------------------------|-------------------------|-------------------|-------|
| | | | | | | (V_b) | (%) |
| 60 | 3 | 4.785 | -4.009 | -12.082 | 0.002 | 12.081 | 106.9 |
| 90 | 5 | 4.303 | -3.883 | -9.753 | 0.041 | 9.713 | 104.5 |
| 120 | 6 | 4.523 | -3.915 | -9.571 | 0.068 | 9.503 | 106.8 |
| 150 | 7 | 3.828 | -4.807 | -6.099 | 0.507 | 5.592 | 85.1 |
| 180 | 8 | 5.515 | -3.401 | -6.348 | 0.005 | 6.342 | 150.0 |
| 210 | 9 | 4.853 | -3.294 | -9.418 | 0.146 | 9.273 | 120.2 |
| 240 | 10 | 4.815 | -3.225 | -5.777 | 0.006 | 5.770 | 138.0 |
| 270 | 12 | 7.223 | -3.300 | -5.202 | 0.218 | 4.984 | 469.9 |
| 300 | 13 | 3.786 | -4.185 | -4.637 | 0.057 | 4.580 | 92.0 |
| 330 | 14 | 3.710 | -4.073 | -6.769 | 0.810 | 5.958 | 94.3 |
| 360 | 15 | 3.701 | -3.096 | -3.870 | 0.029 | 3.841 | 118.7 |
| 390 | 16 | 3.979 | -3.298 | -7.670 | 2.187 | 5.483 | 114.2 |
| 420 | 17 | 2.320 | -5.396 | -2.799 | 0.093 | 2.706 | 46.8 |
| 450 | 18 | 3.390 | -3.785 | -6.686 | 0.906 | 5.780 | 93.6 |
| 480 | 19 | 4.389 | -3.606 | -6.743 | 0.326 | 6.417 | 113.9 |

Table S8. T_IWMC experiment. All values are reported in 10^{-3} m^3 over a period of 30 minutes (Run time is in minutes).

| Upper section | | | | | | |
|----------------------|------|--------------------------|----------------------|------------------------|-------------------------|-----------------------------|
| Run time | DE M | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
| 60 | 3 | 1.600 | -0.516 | 0.000 | 0.000 | 0.000 |
| 90 | 4 | 1.524 | -0.553 | -0.003 | 0.000 | 0.003 |
| 120 | 5 | 1.294 | -0.423 | -0.062 | 0.000 | 0.062 |
| 150 | 6 | 1.320 | -0.380 | -0.001 | 0.000 | 0.001 |
| 180 | 7 | 1.383 | -0.337 | -0.010 | 0.000 | 0.010 |

| | | | | | | |
|-----|----|-------|--------|--------|-------|-------|
| 210 | 8 | 0.495 | -2.022 | -0.499 | 0.000 | 0.499 |
| 240 | 9 | 0.067 | -2.934 | -0.285 | 0.000 | 0.285 |
| 270 | 11 | 0.309 | -1.496 | -0.618 | 0.000 | 0.618 |
| 300 | 12 | 0.050 | -2.686 | -0.206 | 0.000 | 0.206 |
| 330 | 13 | 0.243 | -1.108 | -0.097 | 0.000 | 0.097 |
| 360 | 14 | 0.313 | -0.739 | -1.490 | 0.151 | 1.340 |
| 390 | 15 | 0.246 | -0.838 | -2.745 | 0.003 | 2.742 |
| 420 | 16 | 0.273 | -0.638 | -1.602 | 0.000 | 1.602 |
| 450 | 17 | 0.273 | -2.962 | -0.309 | 0.019 | 0.290 |
| 480 | 18 | 0.476 | -1.369 | -0.904 | 0.001 | 0.903 |

Middle section

| Run time | DE M | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
|----------|------|--------------------------|----------------------|------------------------|-------------------------|-----------------------------|
| 60 | 3 | 1.682 | -2.136 | -1.687 | 0.000 | 1.687 |
| 90 | 4 | 1.411 | -1.829 | -3.157 | 0.000 | 3.157 |
| 120 | 5 | 1.668 | -0.633 | -4.575 | 0.318 | 4.258 |
| 150 | 6 | 1.588 | -0.769 | -5.283 | 0.000 | 5.283 |
| 180 | 7 | 1.334 | -0.836 | -3.001 | 0.003 | 2.998 |
| 210 | 8 | 0.352 | -2.967 | -2.863 | 0.017 | 2.845 |
| 240 | 9 | 0.938 | -2.962 | -3.873 | 0.994 | 2.879 |
| 270 | 11 | 0.791 | -1.751 | -2.602 | 0.015 | 2.586 |
| 300 | 12 | 0.447 | -3.482 | -3.124 | 0.004 | 3.120 |
| 330 | 13 | 0.678 | -2.051 | -5.551 | 0.010 | 5.541 |
| 360 | 14 | 0.294 | -2.736 | -3.209 | 0.009 | 3.199 |
| 390 | 15 | 0.712 | -3.250 | -1.085 | 0.690 | 0.395 |
| 420 | 16 | 0.926 | -3.109 | -1.437 | 0.522 | 0.916 |
| 450 | 17 | 0.837 | -3.403 | -1.709 | 0.026 | 1.682 |
| 480 | 18 | 0.703 | -5.280 | -0.446 | 0.018 | 0.428 |

Lower section

| Run time | DE M | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution (V_b) |
|----------|------|--------------------------|----------------------|------------------------|-------------------------|-----------------------------|
| 60 | 3 | 0.116 | -3.941 | -4.646 | 0.000 | 4.646 |
| 90 | 4 | 0.099 | -1.925 | -3.218 | 0.000 | 3.218 |
| 120 | 5 | 0.397 | -1.817 | -2.224 | 0.003 | 2.221 |
| 150 | 6 | 0.381 | -1.399 | -2.896 | 0.090 | 2.806 |
| 180 | 7 | 1.269 | -1.001 | -5.157 | 0.776 | 4.382 |
| 210 | 8 | 3.897 | -0.789 | -12.035 | 0.087 | 11.947 |
| 240 | 9 | 0.773 | -2.528 | -10.169 | 0.044 | 10.124 |
| 270 | 11 | 0.285 | -4.738 | -3.719 | 0.026 | 3.693 |
| 300 | 12 | 0.605 | -3.440 | -3.396 | 0.112 | 3.283 |
| 330 | 13 | 0.329 | -3.524 | -2.842 | 0.029 | 2.813 |
| 360 | 14 | 0.548 | -2.966 | -3.685 | 0.015 | 3.669 |
| 390 | 15 | 2.586 | -1.425 | -8.784 | 2.222 | 6.562 |
| 420 | 16 | 0.837 | -3.309 | -8.083 | 0.023 | 8.060 |
| 450 | 17 | 2.327 | -1.713 | -2.948 | 0.636 | 2.312 |
| 480 | 18 | 1.212 | -3.872 | -8.081 | 0.217 | 7.864 |

Whole system

| Run time | DEM | Aggradation (A_{vf}) | Erosion (E_{vf}) | Bank erosion (E_b) | Bank deposits (A_b) | Bank contribution | |
|----------|-----|--------------------------|----------------------|------------------------|-------------------------|-------------------|-------|
| | | | | | | (V_b) | (%) |
| 60 | 3 | 3.542 | -6.894 | -6.816 | 0.000 | 6.816 | 67.0 |
| 90 | 4 | 3.156 | -4.456 | -6.614 | 0.000 | 6.614 | 83.6 |
| 120 | 5 | 3.470 | -3.062 | -6.863 | 0.320 | 6.543 | 106.7 |
| 150 | 6 | 3.451 | -2.669 | -8.429 | 0.091 | 8.338 | 110.3 |
| 180 | 7 | 4.123 | -2.324 | -8.272 | 0.779 | 7.493 | 131.6 |
| 210 | 8 | 4.942 | -6.149 | -16.173 | 0.106 | 16.067 | 93.0 |
| 240 | 9 | 1.923 | -8.787 | -15.008 | 1.043 | 13.965 | 67.0 |

| | | | | | | | |
|-----|----|-------|---------|---------|-------|--------|------|
| 270 | 11 | 1.458 | -8.211 | -7.479 | 0.113 | 7.366 | 52.2 |
| 300 | 12 | 1.170 | -9.939 | -7.008 | 0.118 | 6.890 | 44.0 |
| 330 | 13 | 1.364 | -6.912 | -8.515 | 0.041 | 8.474 | 60.4 |
| 360 | 14 | 1.162 | -6.716 | -8.426 | 0.177 | 8.249 | 59.8 |
| 390 | 15 | 3.899 | -5.642 | -12.723 | 2.919 | 9.805 | 84.9 |
| 420 | 16 | 2.097 | -7.379 | -11.129 | 0.548 | 10.581 | 66.7 |
| 450 | 17 | 3.517 | -8.309 | -4.981 | 0.683 | 4.297 | 47.3 |
| 480 | 18 | 2.482 | -10.735 | -9.785 | 0.238 | 9.547 | 53.6 |

Table S9. Fan (a)symmetry measured from the DEMs.

| | Runtime | Upstream side | Central line | Downstream side |
|--------|---------|---------------|--------------|-----------------|
| | (min) | (m) | | |
| T_NCI | 120 | 0.665 | 0.745 | 0.898 |
| | 180 | 0.549 | 0.699 | 0.884 |
| | 240 | 0.595 | 0.638 | 0.78 |
| | 300 | 0.607 | 0.635 | 0.714 |
| | 360 | 0.531 | 0.664 | 0.741 |
| | 420 | 0.523 | 0.626 | 0.706 |
| | 480 | 0.512 | 0.745 | 0.946 |
| | 540 | 0.621 | 0.645 | 0.814 |
| | 600 | 0.63 | 0.741 | 0.905 |
| | 600 | 0.63 | 0.741 | 0.905 |
| T_ISDS | 120 | 0.816 | 1.096 | 1.199 |
| | 180 | 0.874 | 1.081 | 1.178 |
| | 240 | 0.801 | 0.886 | 0.953 |
| | 300 | 0.689 | 0.841 | 0.951 |
| | 360 | 0.866 | 0.978 | 1.031 |
| | 420 | 0.844 | 1.071 | 1.244 |
| | 480 | 1.046 | 1.079 | 1.181 |
| | 540 | 0.996 | 1.075 | 1.286 |
| T_DWIW | 120 | 0.829 | 0.994 | 1.181 |
| | 180 | 0.845 | 0.887 | 0.935 |
| | 240 | 0.698 | 0.799 | 0.896 |
| | 300 | 0.697 | 0.832 | 0.948 |
| | 360 | 0.804 | 0.949 | 1.066 |
| | 420 | 0.772 | 0.869 | 1.199 |
| | 480 | 0.82 | 1.067 | 1.211 |
| | 540 | 0.859 | 1.111 | 1.032 |
| T_NC2 | 120 | 0.898 | 0.956 | 1.023 |
| | 180 | 0.841 | 0.972 | 1.101 |
| | 240 | 0.724 | 0.982 | 1.057 |
| | 300 | 0.823 | 1.068 | 1.141 |
| | 360 | 0.768 | 0.889 | 1.016 |
| | 420 | 0.784 | 1.077 | 1.156 |
| | 480 | 0.7 | 0.942 | 1.122 |
| | 480 | 0.692 | 0.796 | 1.08 |
| T_IWMC | 120 | 0.848 | 0.961 | 1.023 |
| | 180 | 0.803 | 0.891 | 1.031 |
| | 240 | 0.801 | 0.862 | 0.997 |
| | 300 | 0.842 | 0.977 | 1.071 |
| | 360 | 0.741 | 0.811 | 0.996 |
| | 420 | 0.788 | 0.940 | 1.055 |
| | 480 | 0.692 | 0.796 | 1.08 |

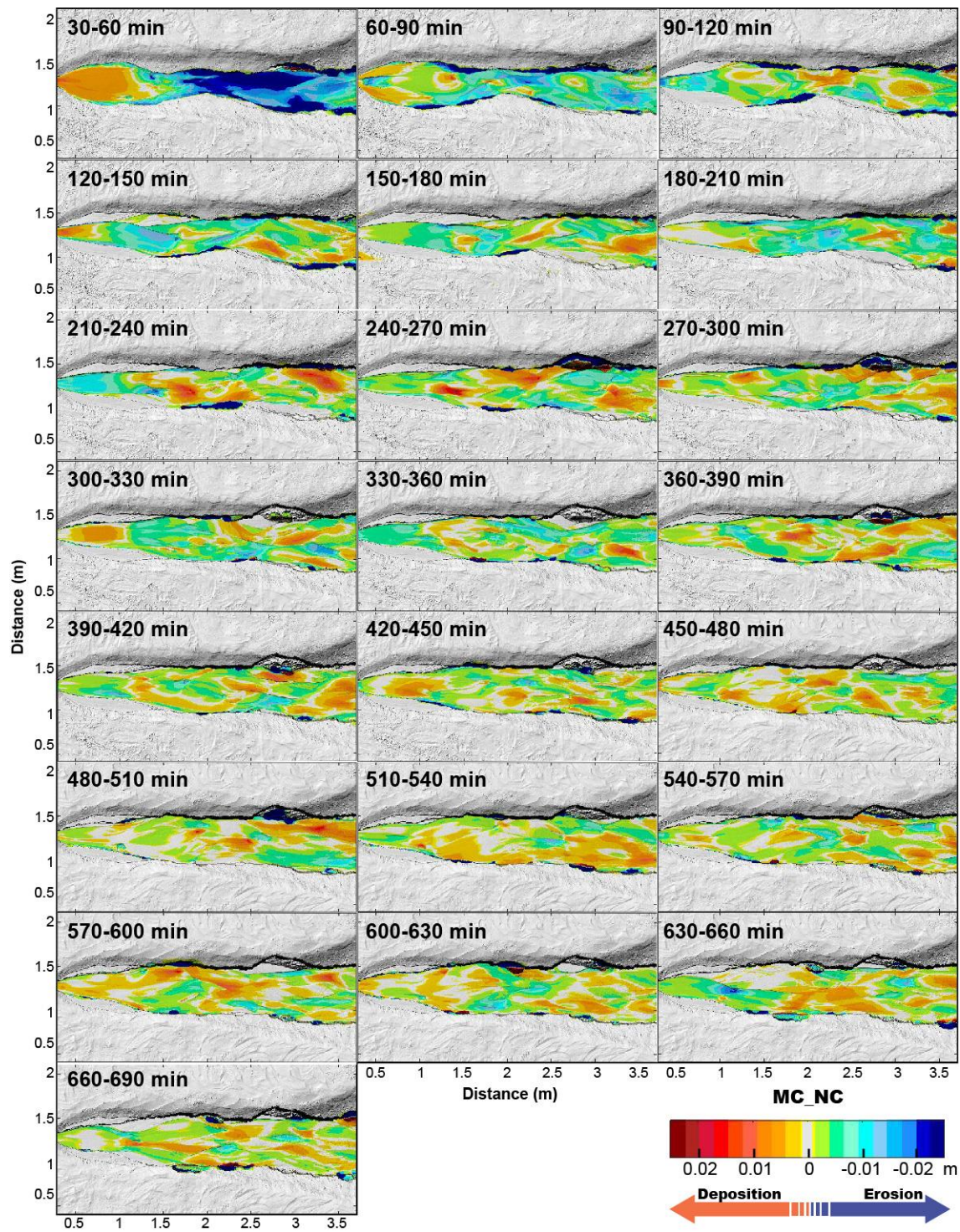


Figure S1. Sediment transfer dynamics from DoDs analysis. Variations between -0.001 and $+0.001$ m are considered as “no change” (in gray) to account for the DEMs accuracy (i.e., 1 mm resolution).

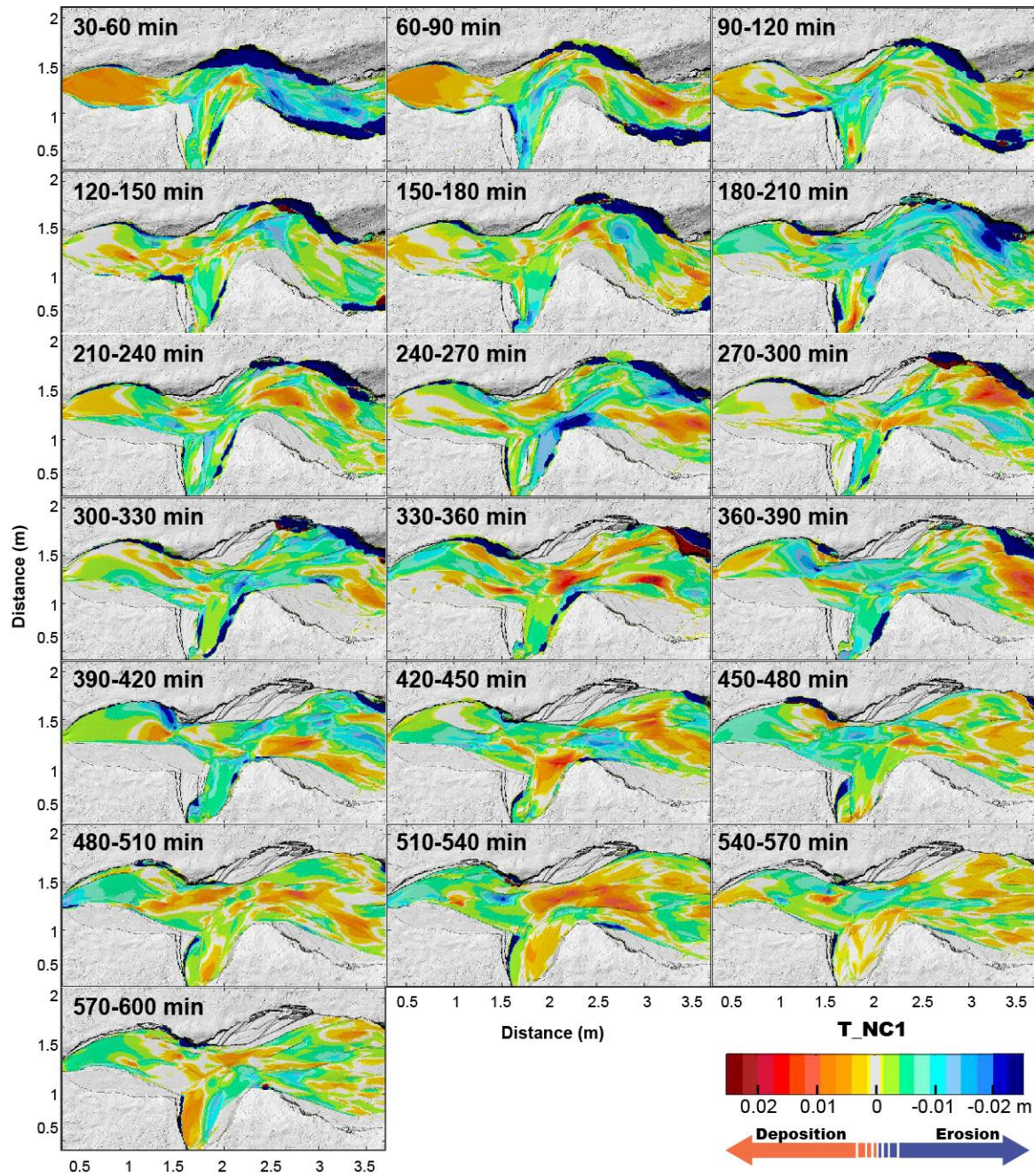


Figure S2. Sediment transfer dynamics from DoDs analysis. Variations between -0.001 and $+0.001$ m are considered as “no change” (in gray) to account for the DEMs accuracy (i.e., 1 mm resolution).

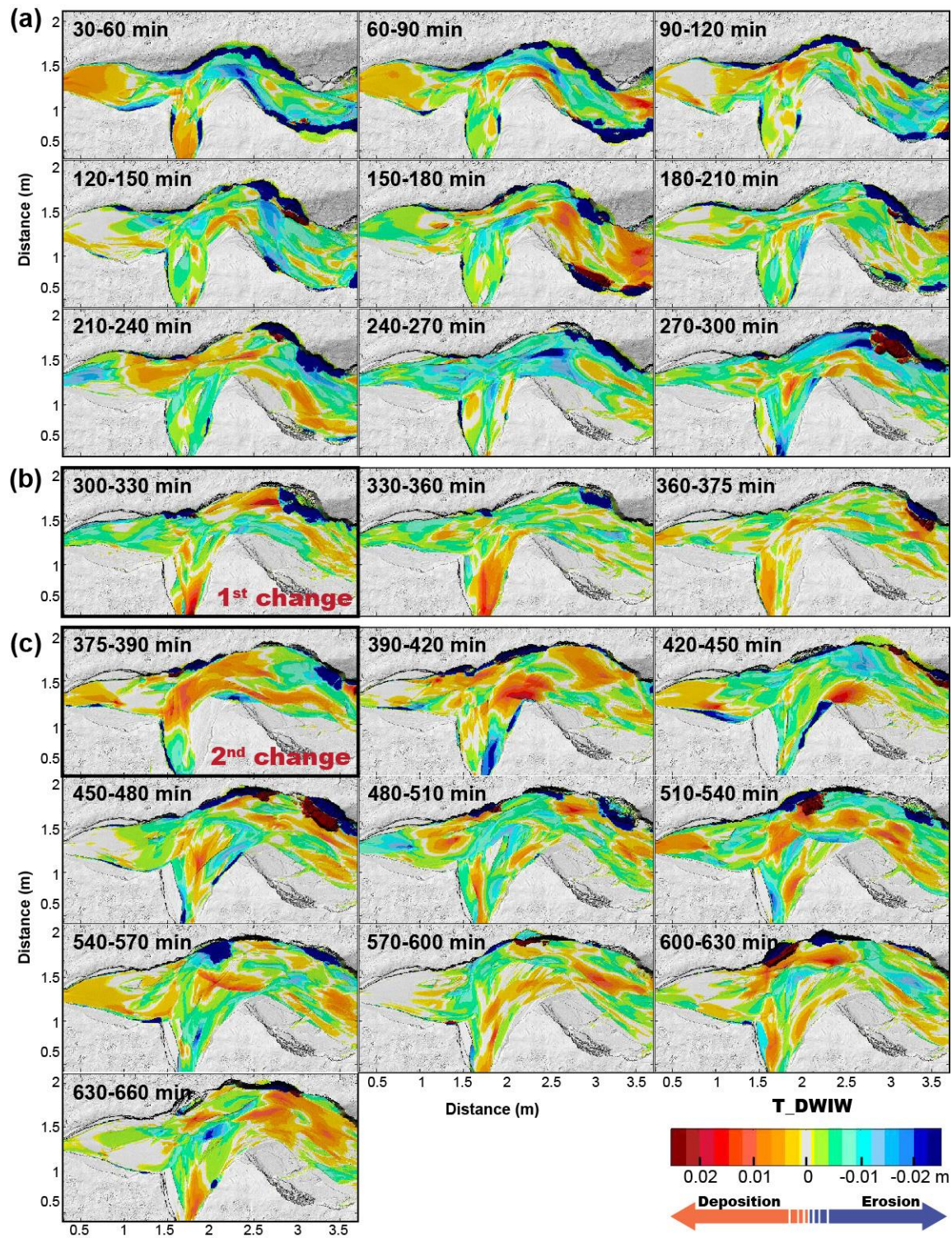


Figure S3. Sediment transfer dynamics from DoDs analysis. Variations between -0.001 and $+0.001$ m are considered as “no change” (in gray) to account for the DEMs accuracy (i.e., 1 mm resolution).

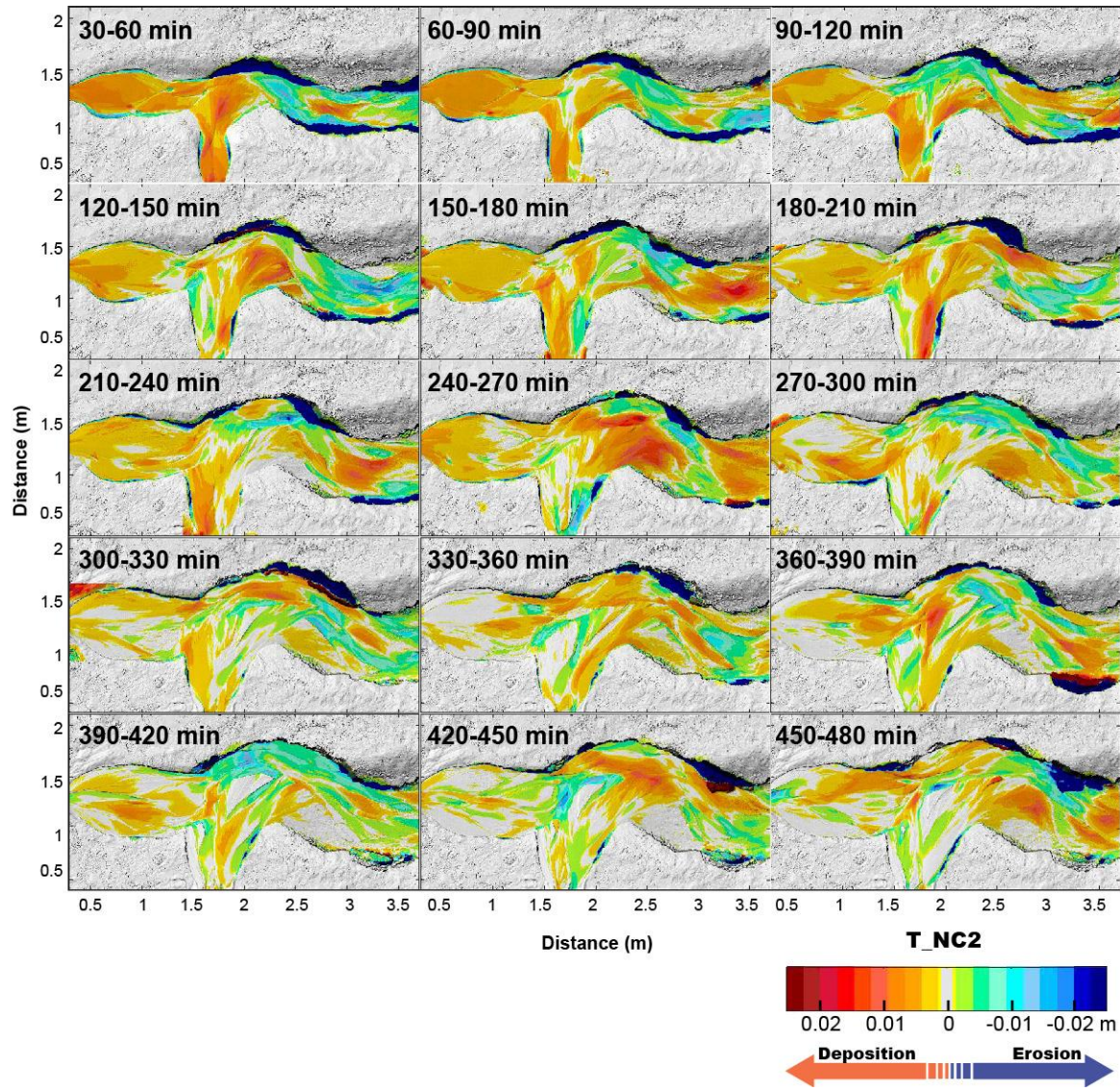


Figure S4. Sediment transfer dynamics from DoDs analysis. Variations between -0.001 and +0.001 m are considered as “no change” (in gray) to account for the DEMs accuracy (i.e., 1 mm resolution).

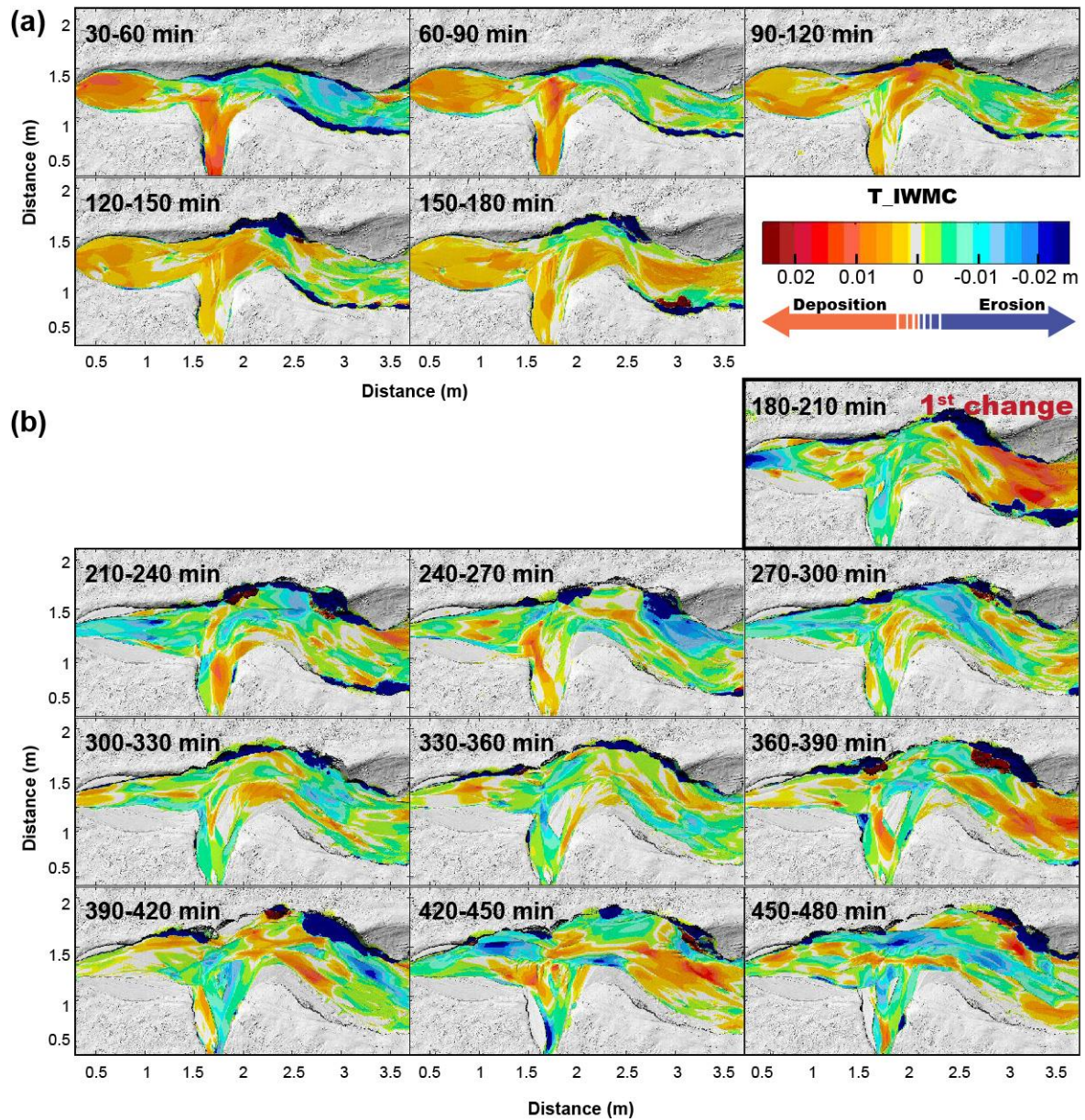


Figure S5. Sediment transfer dynamics from DoDs analysis. Variations between -0.001 and $+0.001$ m are considered as “no change” (in gray) to account for the DEMs accuracy (i.e., 1 mm resolution).

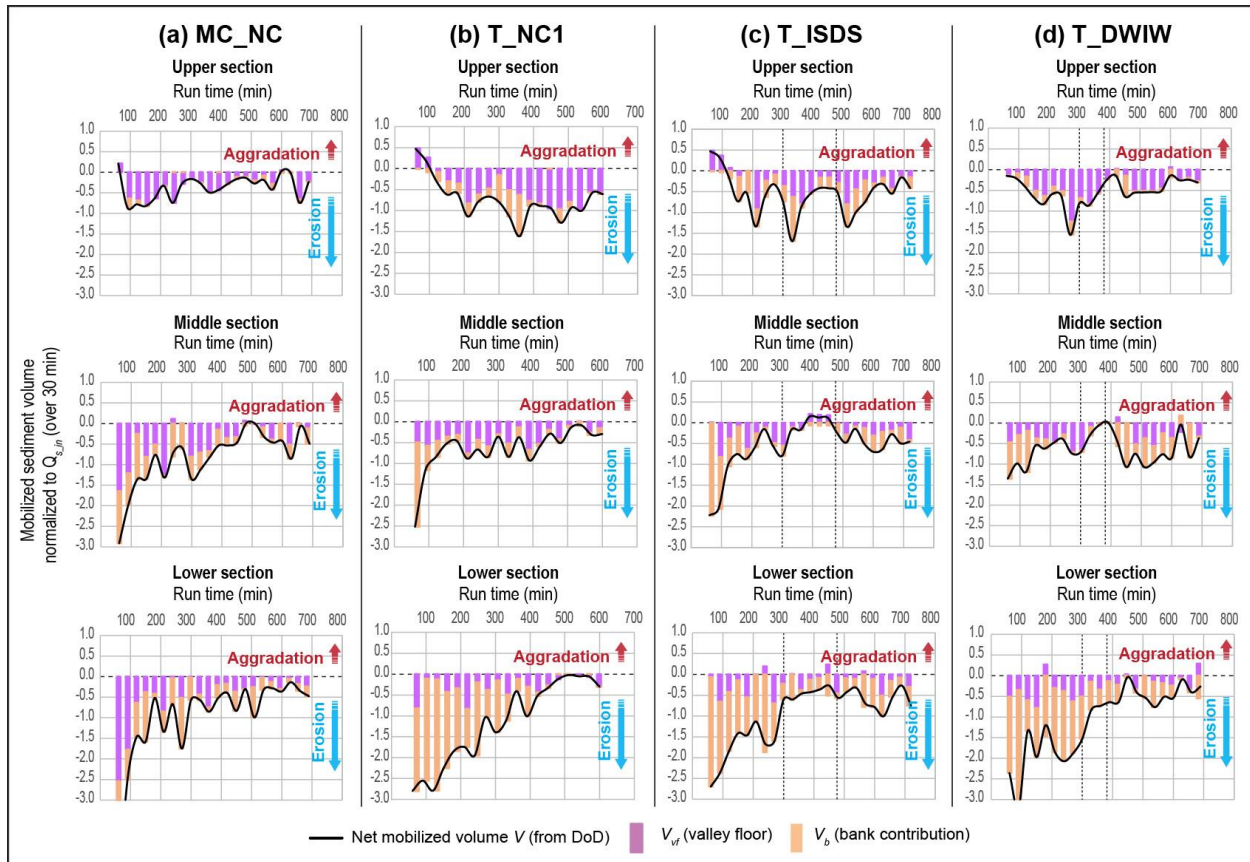


Figure S6. Net volume of sediment mobilized in the upper, middle, and lower sections (normalized to $Q_{s,in}$). Net V values are in black; bank contribution (V_b) is in orange, whereas valley floor (V_{af}) is in violet.

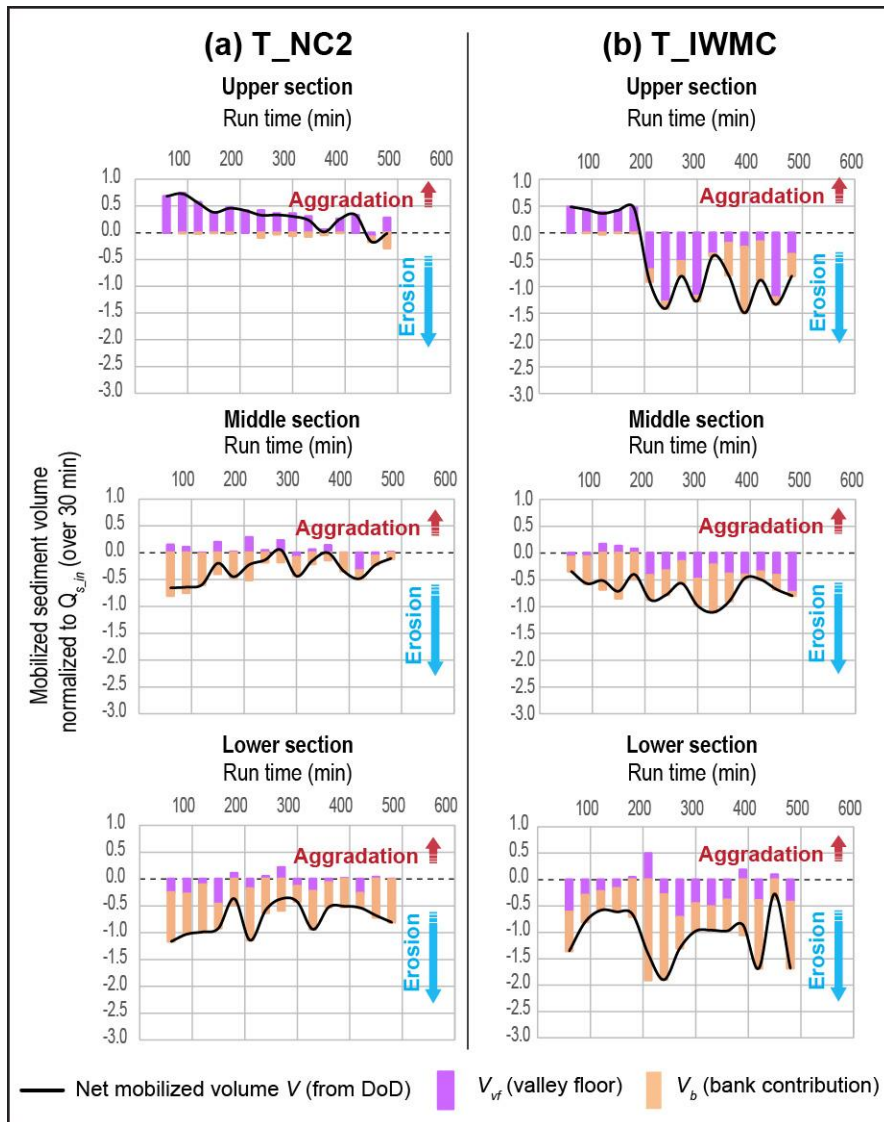


Figure S7. Net volume of sediment mobilized in the upper, middle, and lower sections (normalized to $Q_{s,in}$). Net V values are in black; bank contribution (V_b) is in orange, whereas valley floor (V_{vf}) is in violet.